



*Incorporating 3D Mechansims into
2D Dislocation Dynamics*

A. AMINE BENZERGA

benzerga@aero.tamu.edu

Department of Aerospace Engineering, Texas A&M University

Y. BRÉCHET

LTPCM, Grenoble, France

A. NEEDLEMAN

Brown University, Providence, RI

E. VAN DER GIESSEN

Gröningen, The Netherlands





Background

- Micron-scale Plastic Behaviour:
 - Confined plasticity: e.g. fracture, contact
 - Inelastic deformation in small volumes
- 2D Dislocation Dynamics (“out-of-plane”)
Lepinoux & Kubin; Gulluoglu et al.; Amodeo & Ghoniem; Lubarda et al.
- 3D Dislocation Dynamics: (*mostly periodic BC*) Devincere & Kubin; Canova et al.; Schwarz; Ghoniem et al.; Zbib et al.; Weygand et al.
- 2D Framework by van der Giessen & Needleman
Solve BVP with plastic flow \equiv glide of \perp 's
composites; bending; stationary cracks; stress in thin films; fatigue



What?

Include 3D physics in 2D framework

- In discrete dislocation plasticity the long-range interactions are directly taken into account. Short-range interactions are supplied through constitutive rules.
- Rules are needed in 2D as well as in 3D simulations but more rules are generally needed in 2D.
- More rules to incorporate more physics
 - *line tension*
 - *junction formation*
 - *dynamic sources*
 - *dynamic obstacles*

Why?

- Point sources (and obstacles) are not physical;
Real sources are dislocation segments



Why?

- Point sources (and obstacles) are not physical;
Real sources are dislocation segments
- In the previous 2D framework, the density of sources does not evolve (*idem* for obstacles)



Why?

- Point sources (and obstacles) are not physical;
Real sources are dislocation segments
- In the previous 2D framework, the density of sources does not evolve (*idem* for obstacles)
- As a consequence, hardening is quite limited



Why?

- Point sources (and obstacles) are not physical;
Real sources are dislocation segments
- In the previous 2D framework, the density of sources does not evolve (*idem* for obstacles)
- As a consequence, hardening is quite limited
- It is also important to identify the parameters affecting energy storage and dissipation



Why?

- Point sources (and obstacles) are not physical;
Real sources are dislocation segments
- In the previous 2D framework, the density of sources does not evolve (*idem* for obstacles)
- As a consequence, hardening is quite limited
- It is also important to identify the parameters affecting energy storage and dissipation
- 3D Dislocation Dynamics
performance limited by computing power



Outline

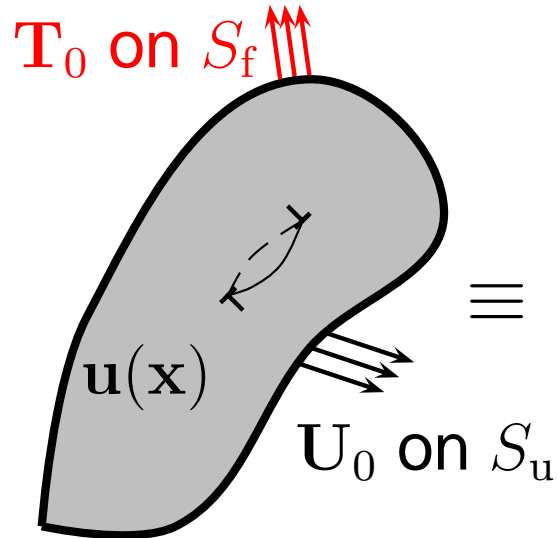
1. Discrete Dislocation Plasticity
2. 3D Rules in 2D Framework
3. Work-Hardening

Benzerga, Bréchet, Needleman & Van der Giessen (MSMSE) 2004

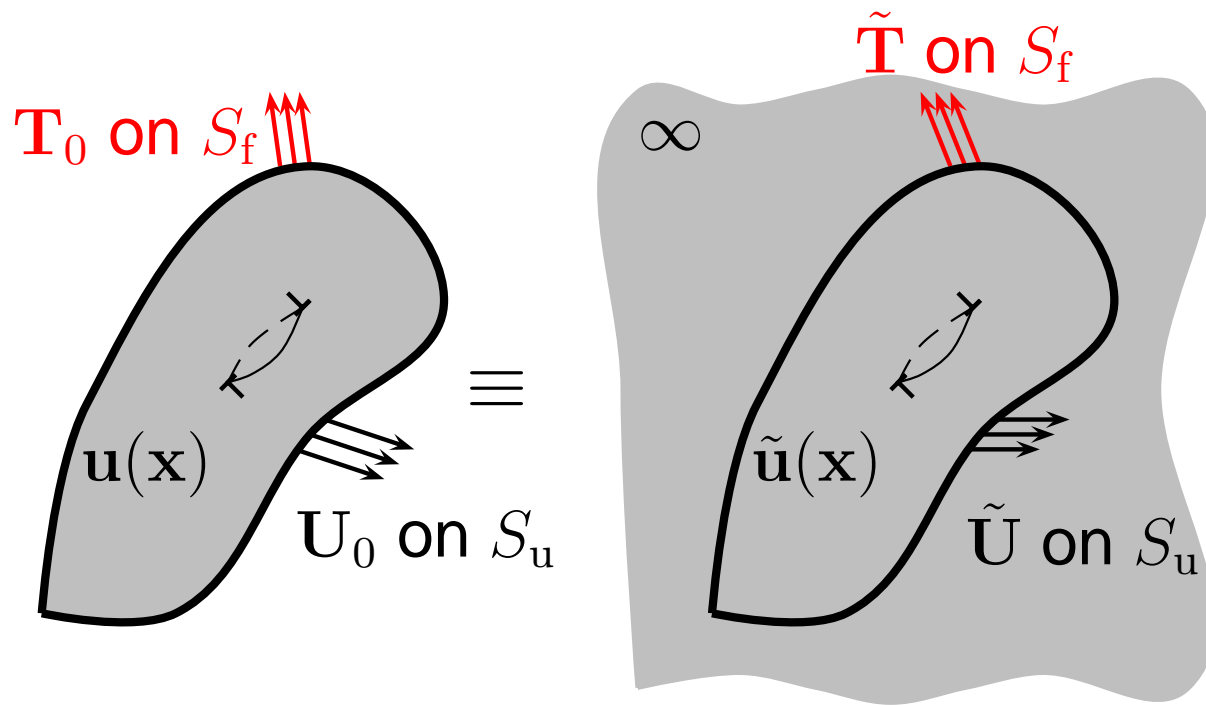
4. Relation to geometric hardening and GNDs
5. The Stored Energy of Cold Work



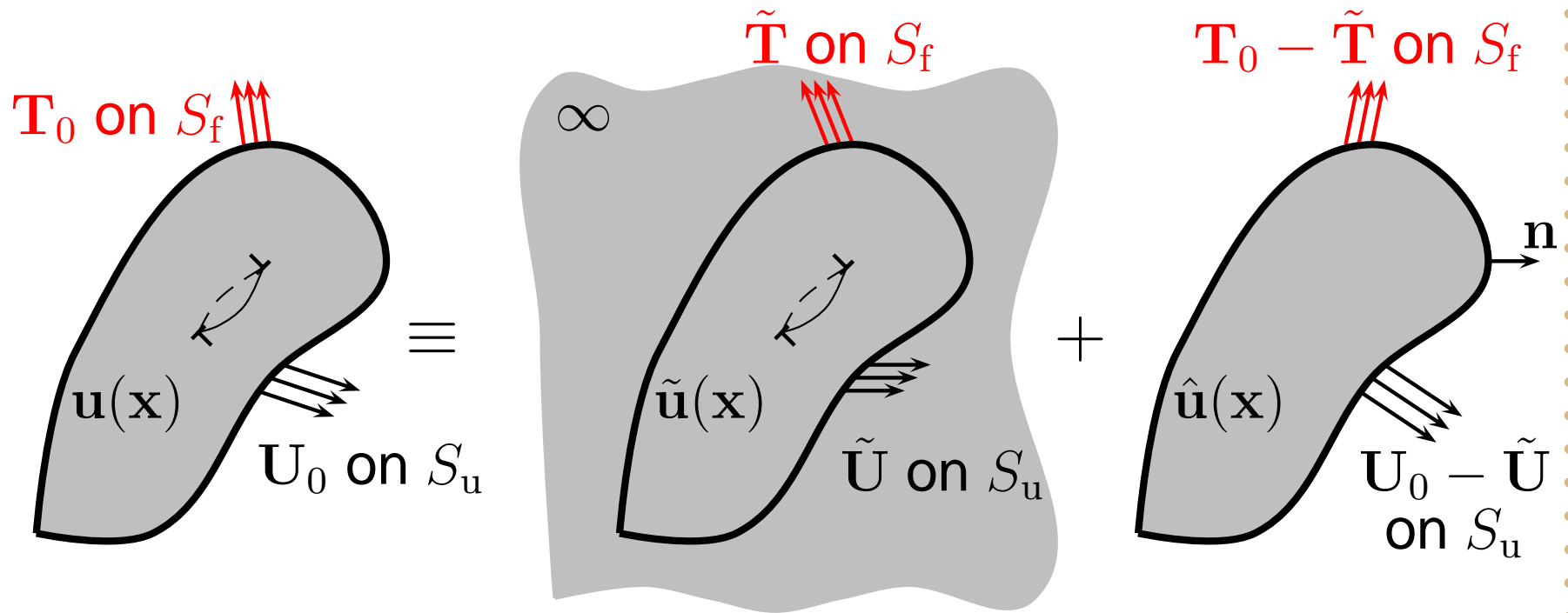
Discrete Dislocation Plasticity



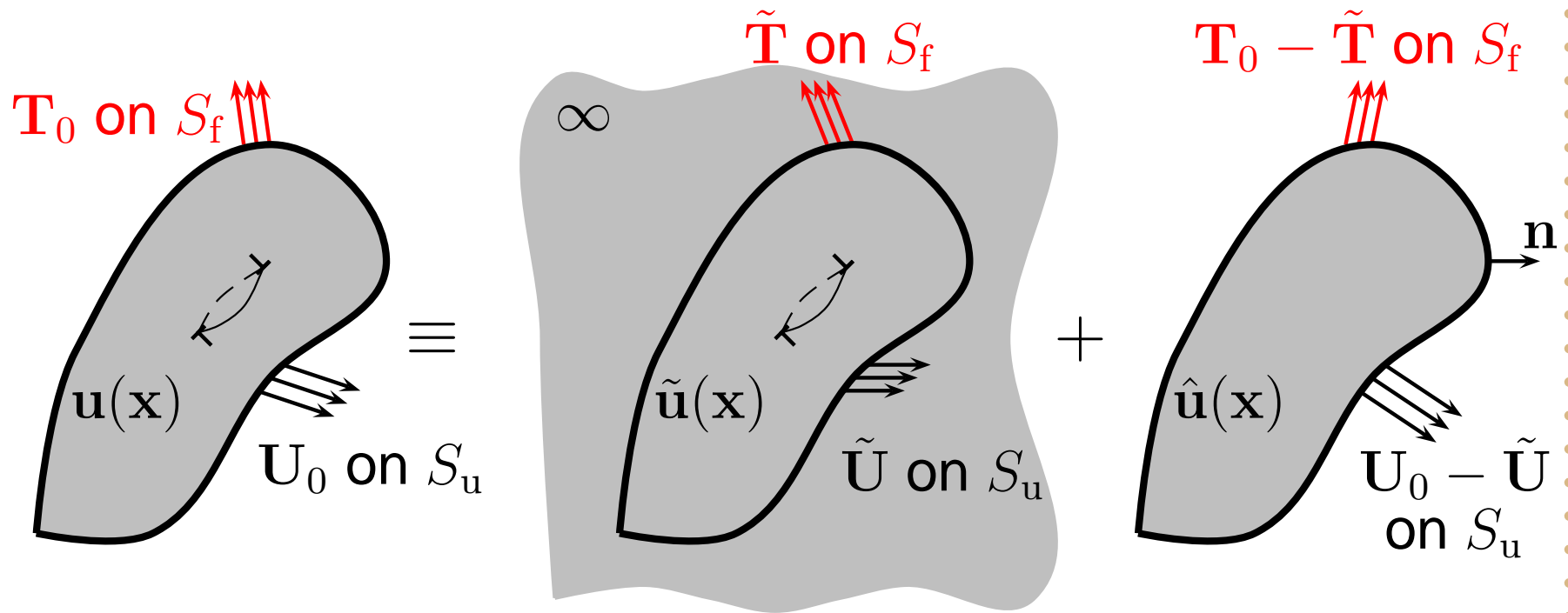
Discrete Dislocation Plasticity



Discrete Dislocation Plasticity

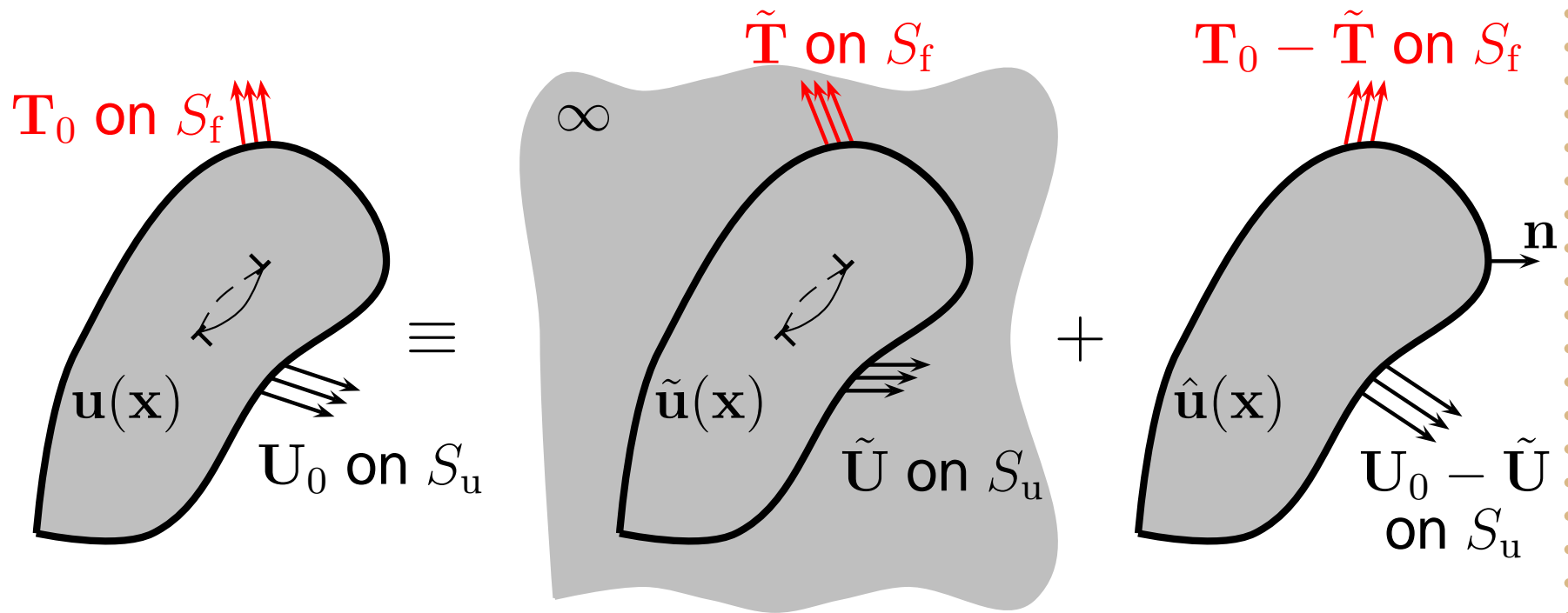


Discrete Dislocation Plasticity



$$\nabla \cdot \hat{\boldsymbol{\sigma}} = \mathbf{0} \quad ; \quad \hat{\boldsymbol{\epsilon}} = \nabla \otimes \hat{\mathbf{u}} \quad ; \quad \hat{\boldsymbol{\sigma}} = \mathcal{L} : \hat{\boldsymbol{\epsilon}} \quad \text{for } \mathbf{x} \in V$$

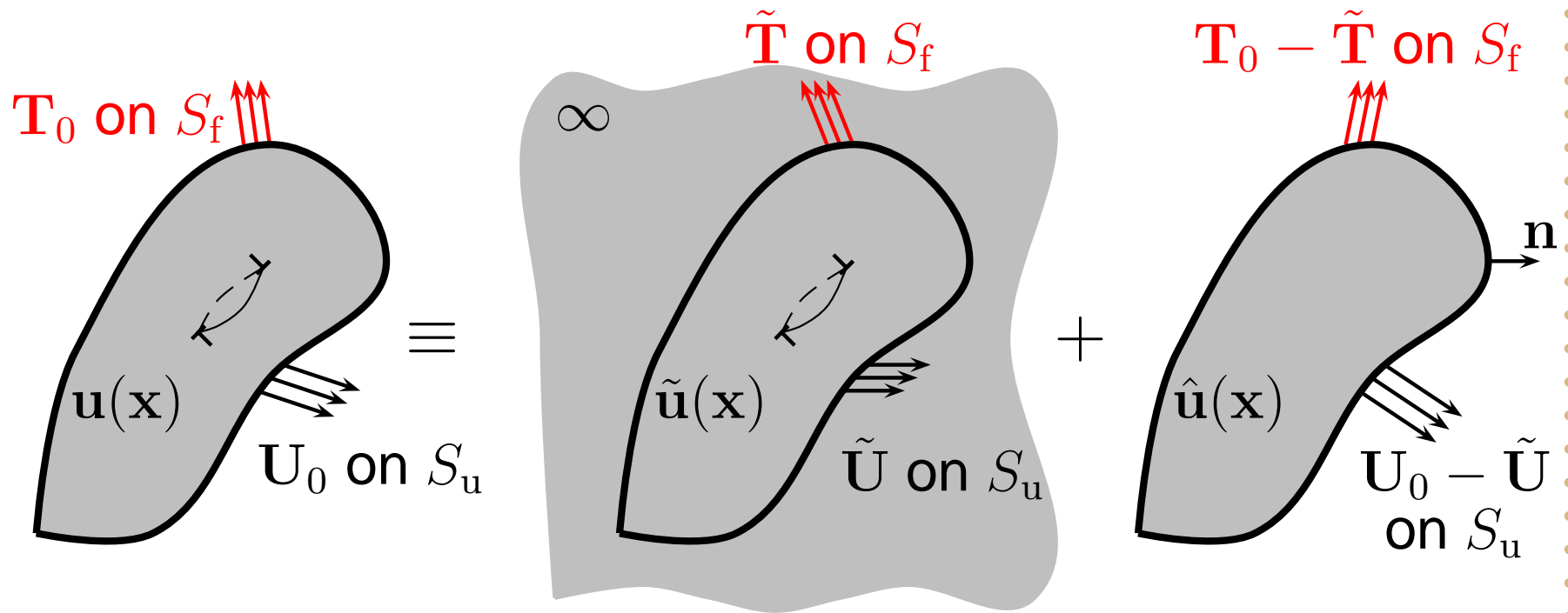
Discrete Dislocation Plasticity



$$\nabla \cdot \hat{\boldsymbol{\sigma}} = \mathbf{0} \quad ; \quad \hat{\boldsymbol{\epsilon}} = \nabla \otimes \hat{\mathbf{u}} \quad ; \quad \hat{\boldsymbol{\sigma}} = \mathcal{L} : \hat{\boldsymbol{\epsilon}} \quad \text{for } \mathbf{x} \in V$$

$$\mathbf{n} \cdot \hat{\boldsymbol{\sigma}} = \mathbf{T}_0 - \mathbf{n} \cdot \tilde{\boldsymbol{\sigma}} \quad \text{for } \mathbf{x} \in S_f \quad ; \quad \hat{\mathbf{u}} = \mathbf{U}_0 - \tilde{\mathbf{U}} \quad \text{for } \mathbf{x} \in S_u$$

Discrete Dislocation Plasticity

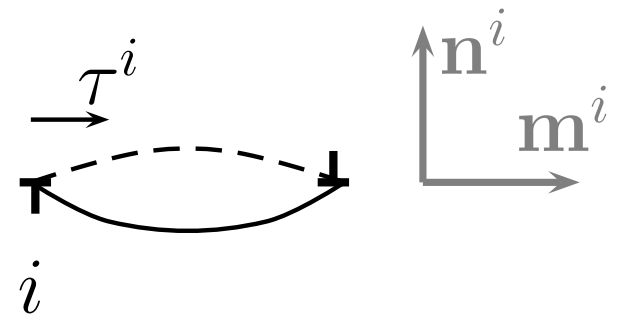


$$\mathbf{u}(\mathbf{x}) = \tilde{\mathbf{u}}(\mathbf{x}) + \hat{\mathbf{u}}(\mathbf{x}) \quad ; \quad \boldsymbol{\epsilon} = \tilde{\boldsymbol{\epsilon}} + \hat{\boldsymbol{\epsilon}} \quad ; \quad \boldsymbol{\sigma} = \tilde{\boldsymbol{\sigma}} + \hat{\boldsymbol{\sigma}}$$

2D Dislocation Dynamics

- **Nucleation:** Static initial sources of constant strength and nucleation time.
- **The Peach–Koehler force:**

$$f^i = \mathbf{n}^i \cdot \left(\hat{\boldsymbol{\sigma}} + \sum_{j \neq i} \boldsymbol{\sigma}^j \right) \cdot \mathbf{b}^i$$



- **Viscous drag:**

$$Bv^i = f^i \approx \tau^i b^i$$

$$b^i \equiv (\mathbf{b}^i \times \mathbf{t}^i) \cdot \mathbf{n}^i$$

B : phonon drag coefficient



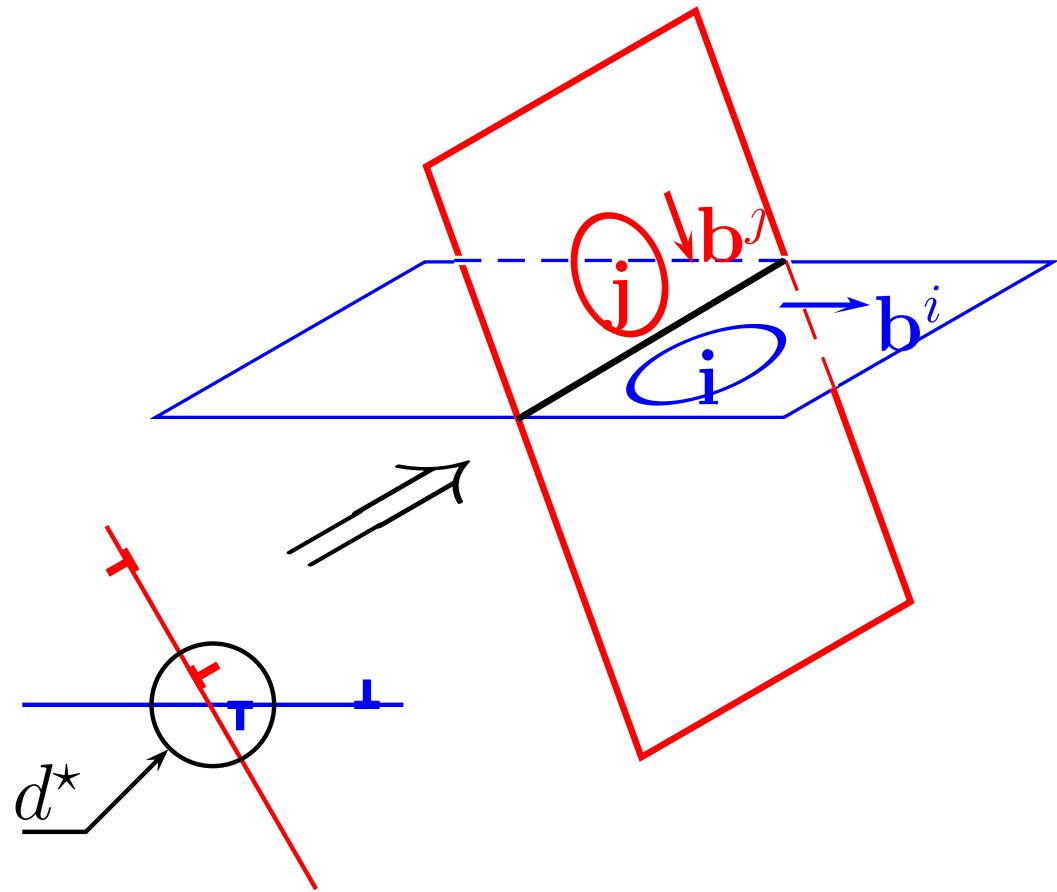
Incorporating 3D Mechanisms into 2D Dislocation Dynamics

Constitutive rules are needed for:

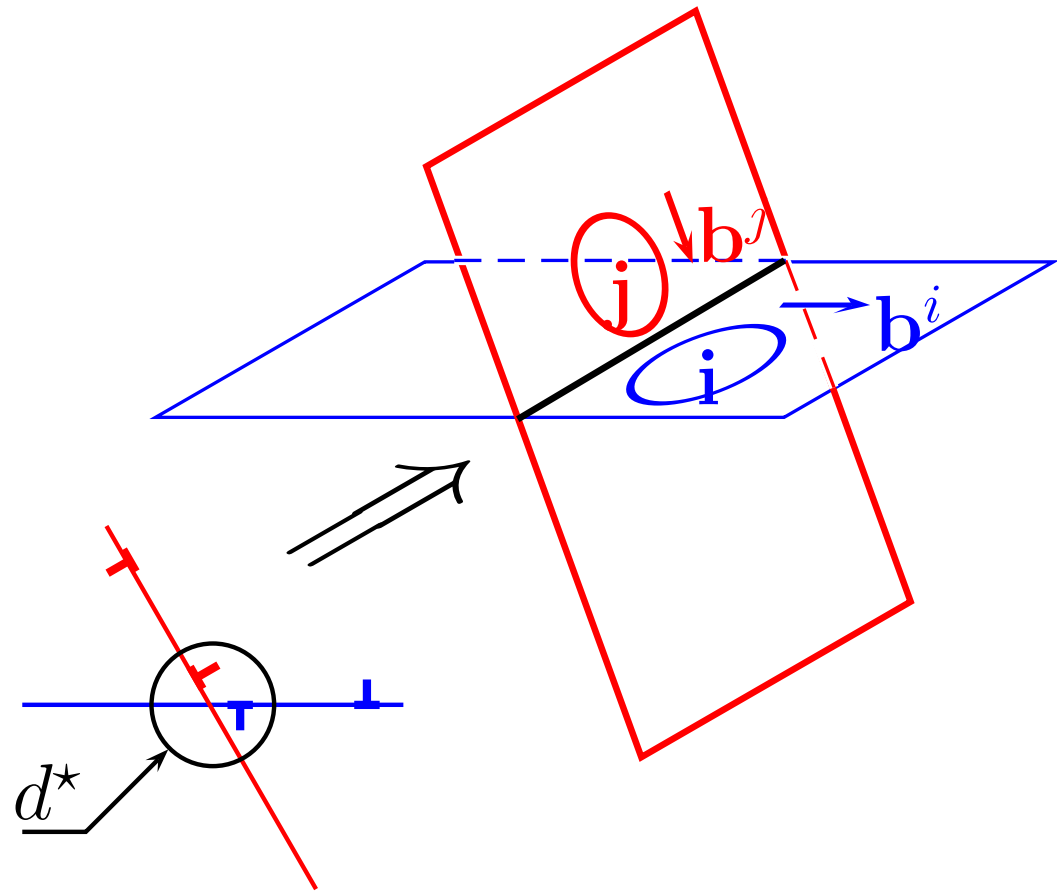
- Junction Formation
- Dynamic Sources
- Dynamic Obstacles
- Higher-order Interactions
- Line Tension



Junction Formation

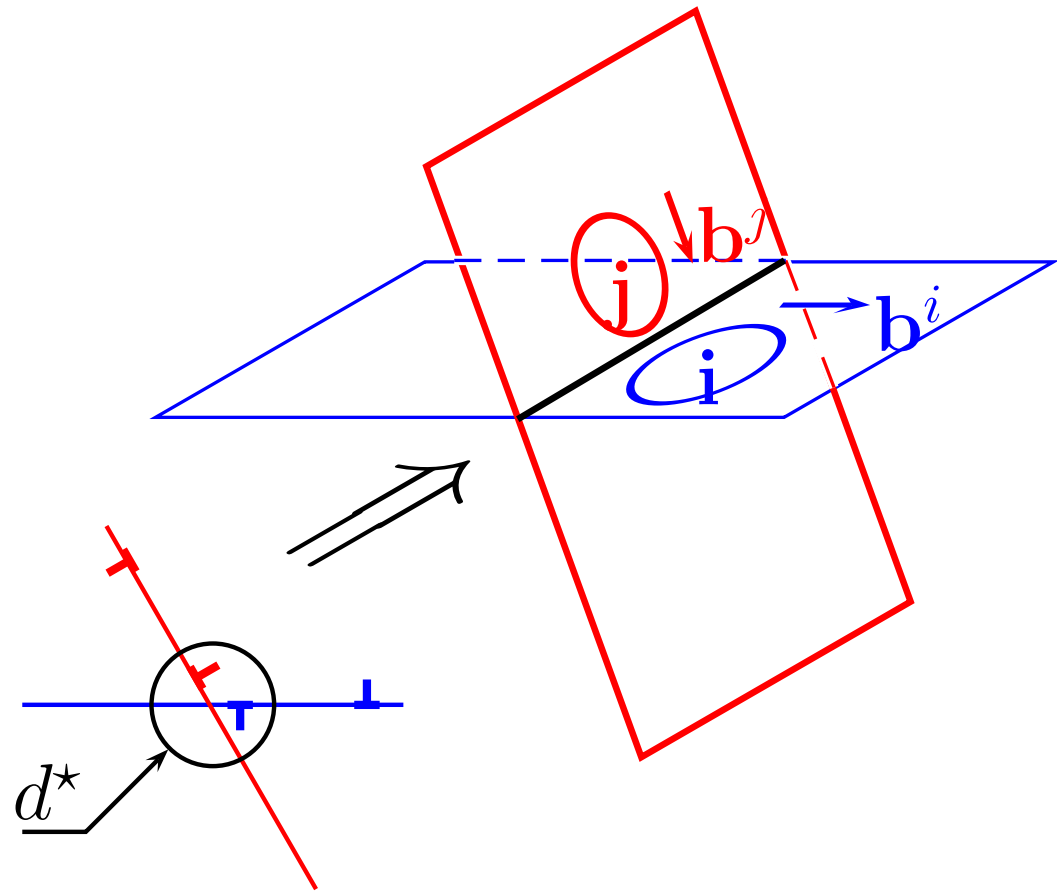


Junction Formation



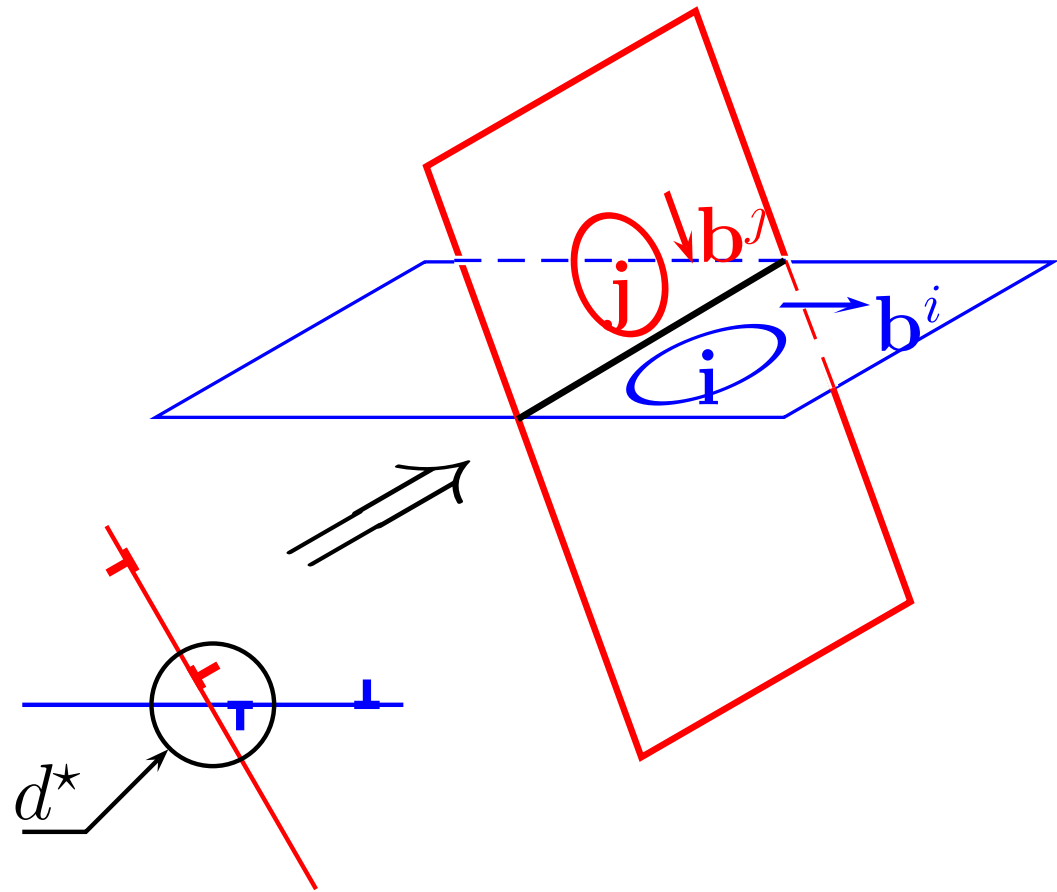
A stable junction is an *anchoring point*...

Junction Formation



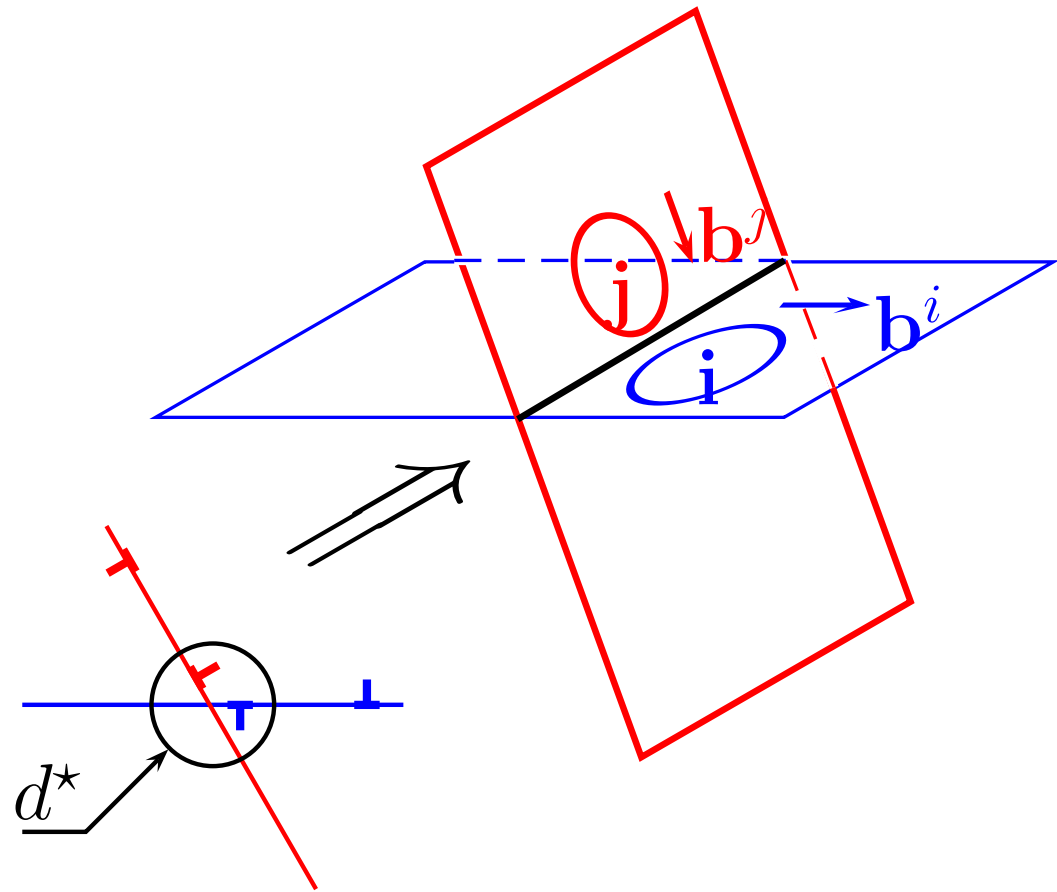
A breakable junction is an *obstacle*...

Junction Formation



Presumably, cross-slip favors anchoring points...

Junction Formation

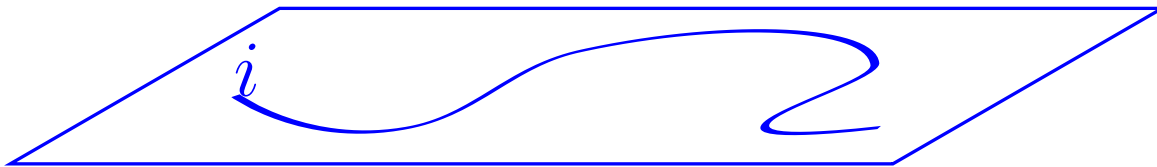


in 2D, anchoring points have formation probability p .

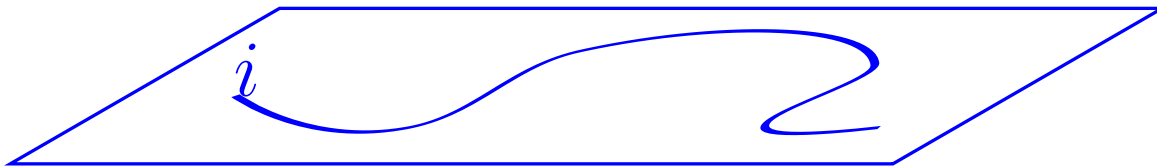
Dynamic Sources



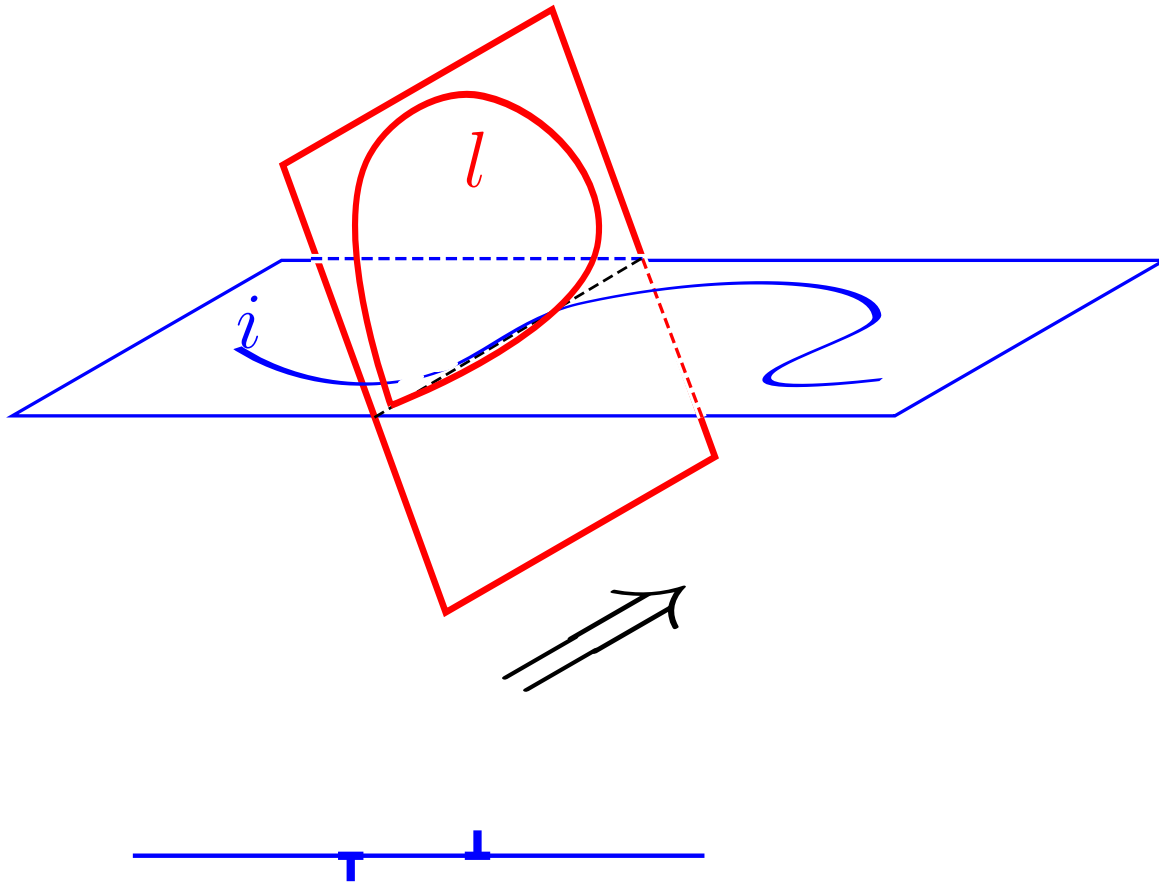
Dynamic Sources



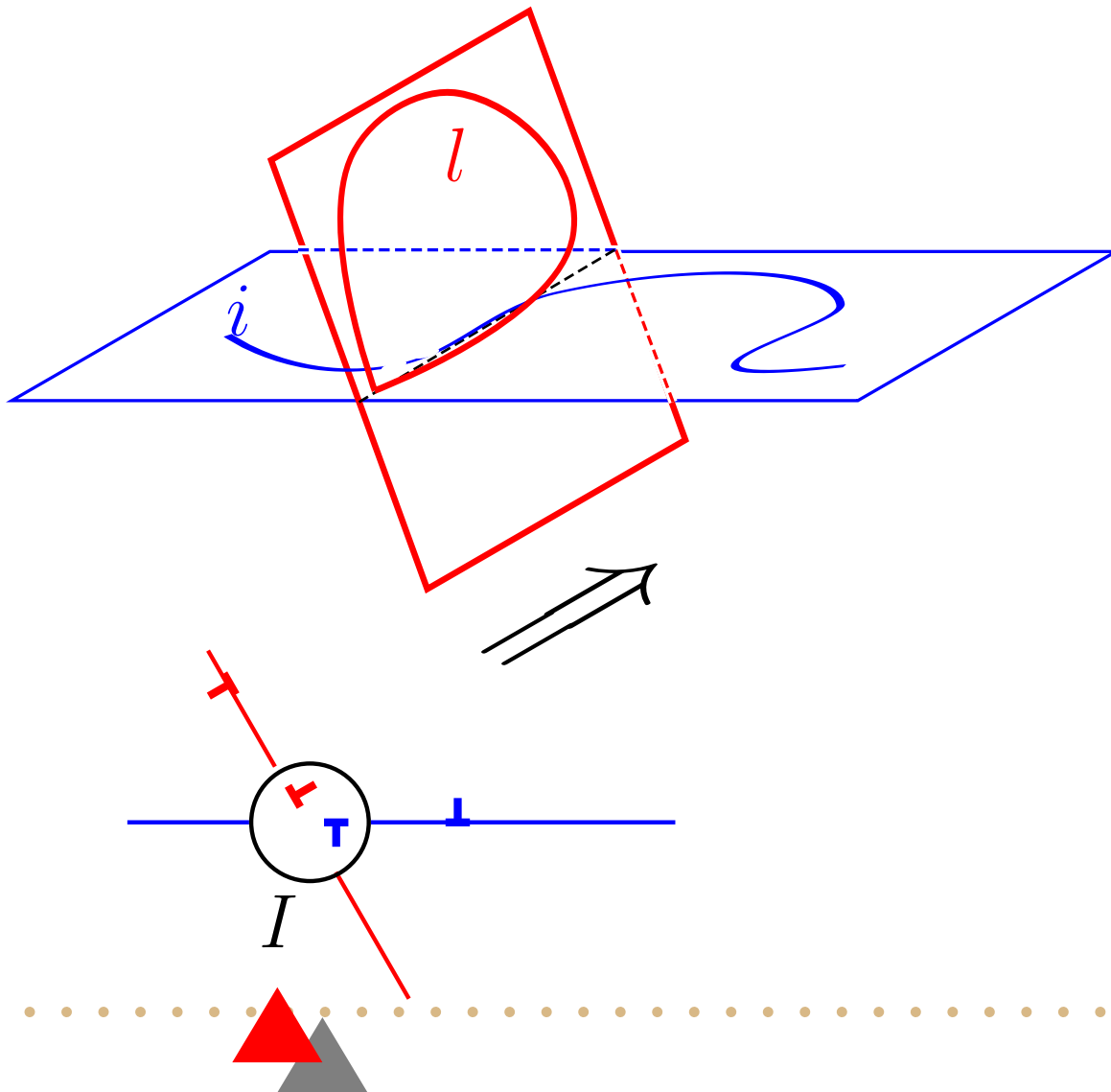
Dynamic Sources



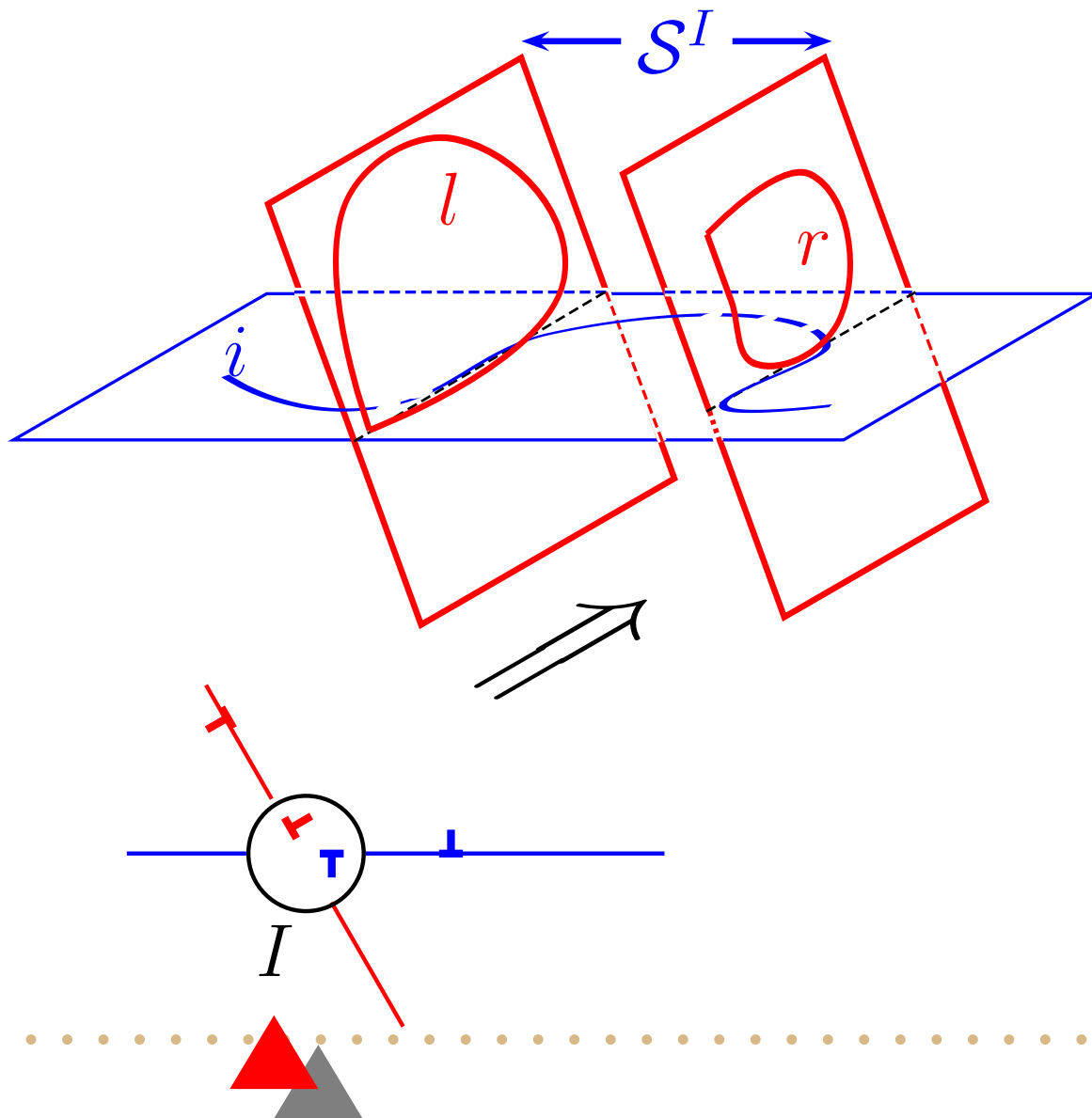
Dynamic Sources



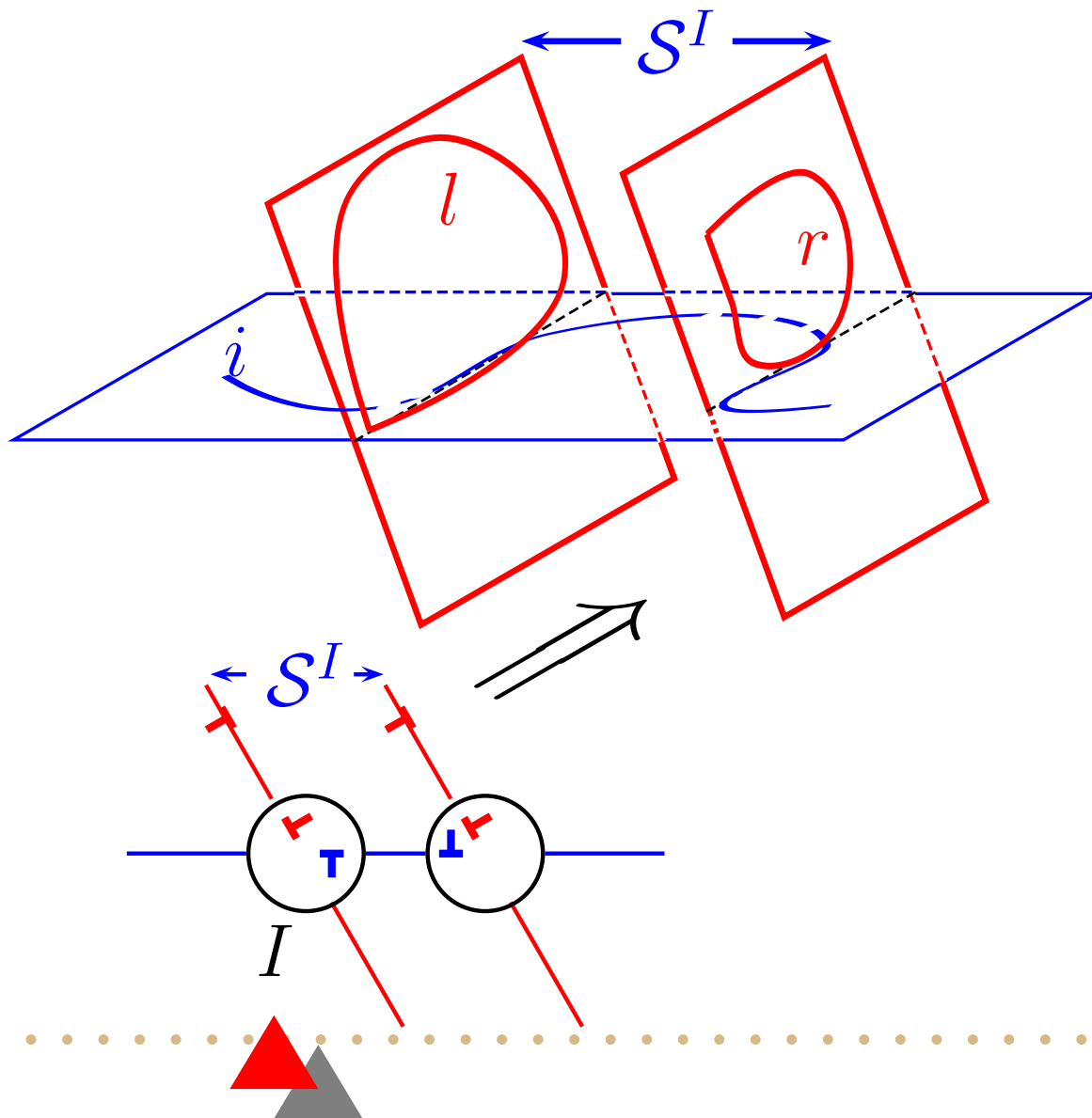
Dynamic Sources



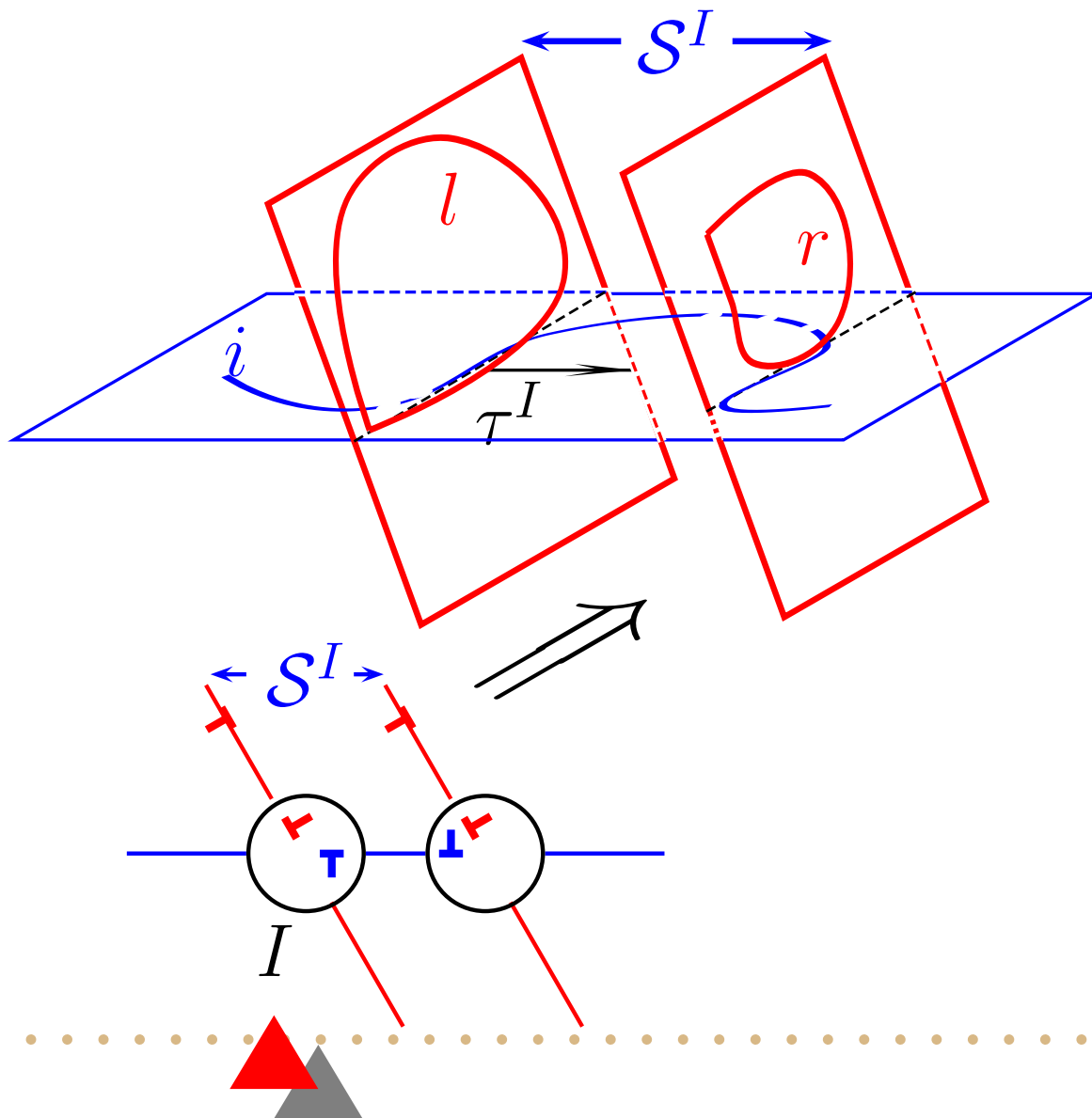
Dynamic Sources



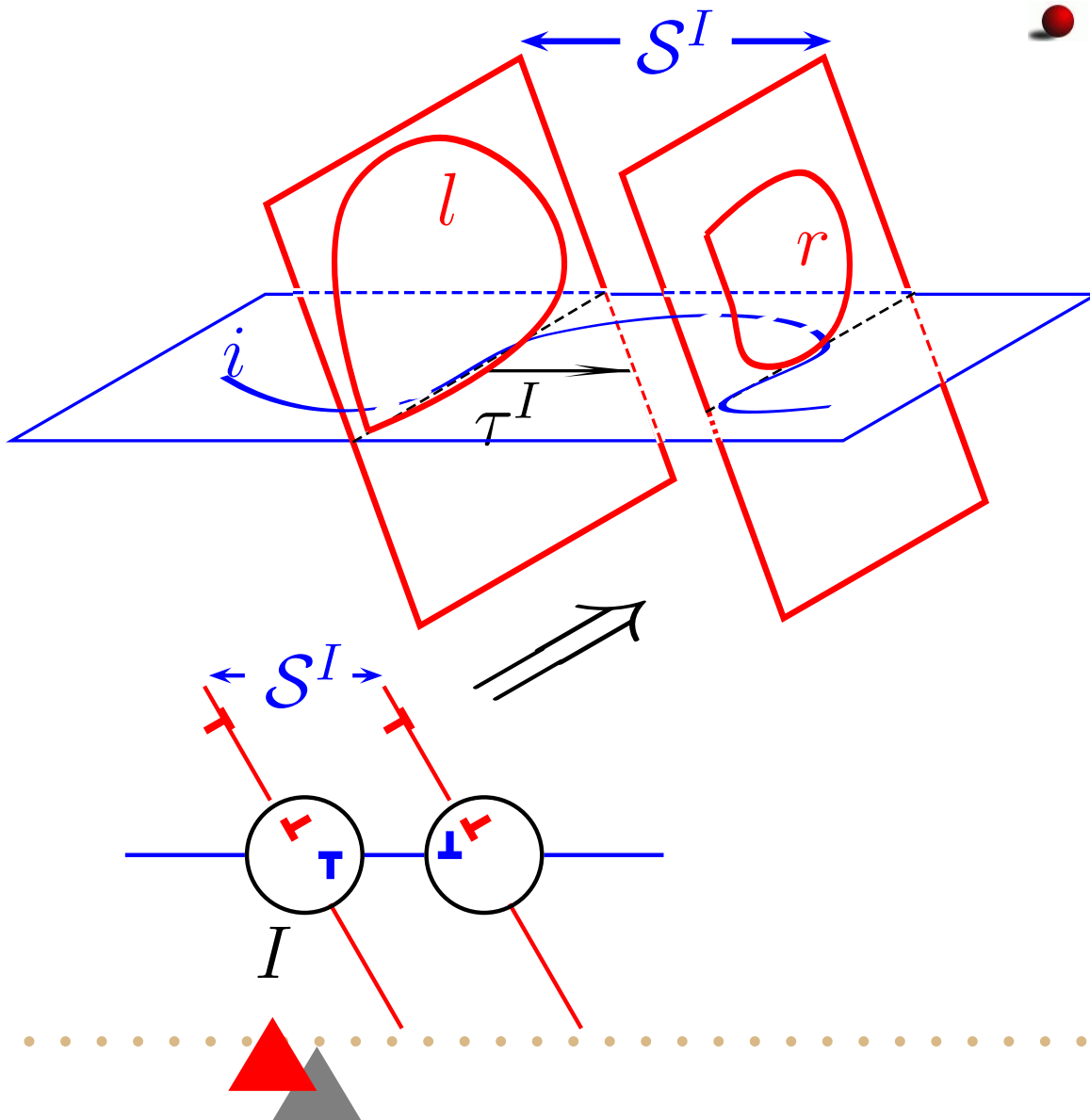
Dynamic Sources



Dynamic Sources



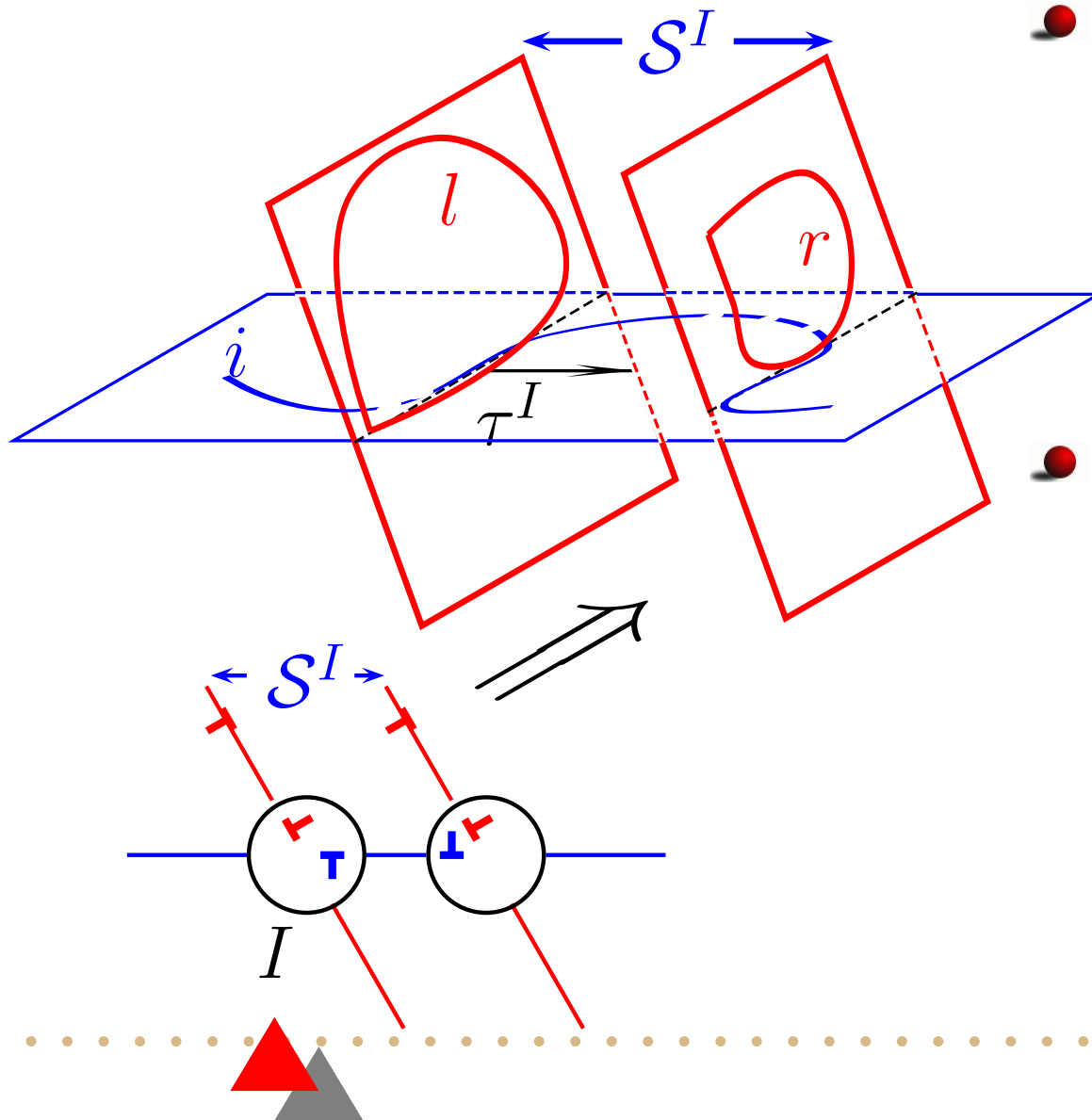
Dynamic Sources



● Critical Stress

$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

Dynamic Sources



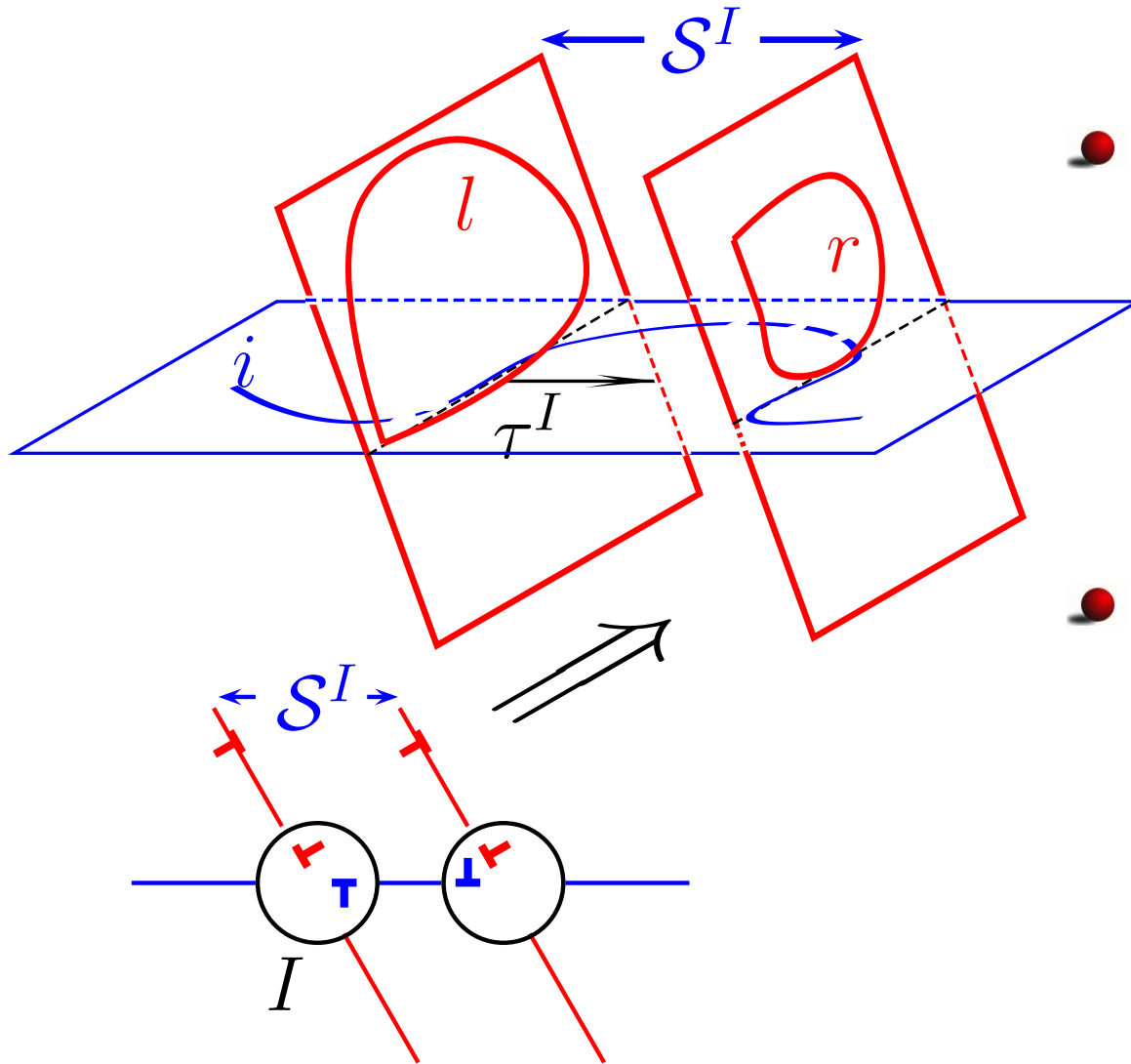
- **Critical Stress**

$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

- **Critical Time**

$$t_{\text{nuc}}^I = B\mathcal{F}(\xi) \frac{S^I}{|\tau^I| b^i}$$

Dynamic Sources



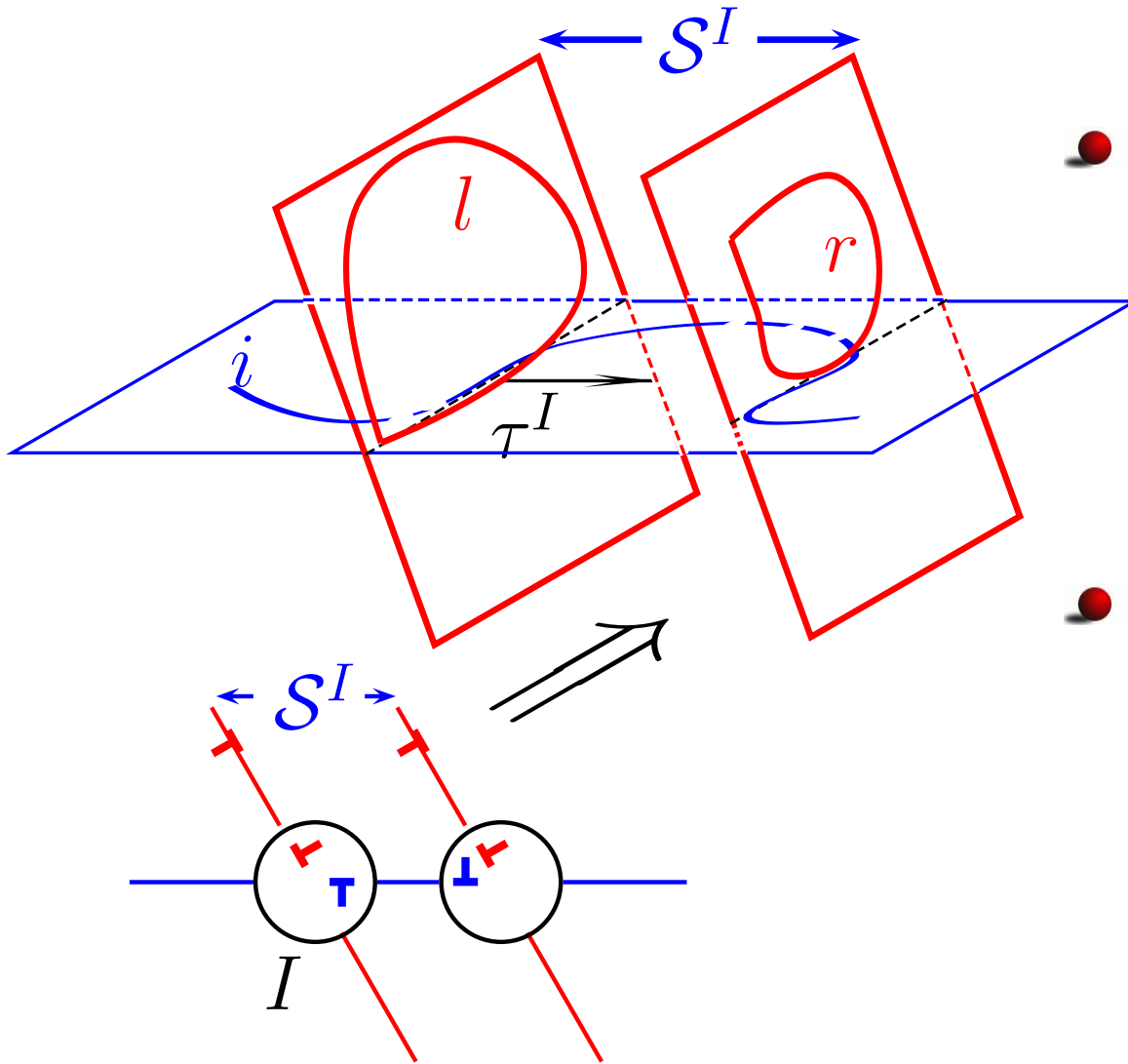
● Critical Stress

$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

● Critical Time

$$t_{\text{nuc}}^I = \underbrace{B\mathcal{F}(\xi)}_{\gamma} \frac{S^I}{|\tau^I| b^i}$$

Dynamic Sources



● Critical Stress

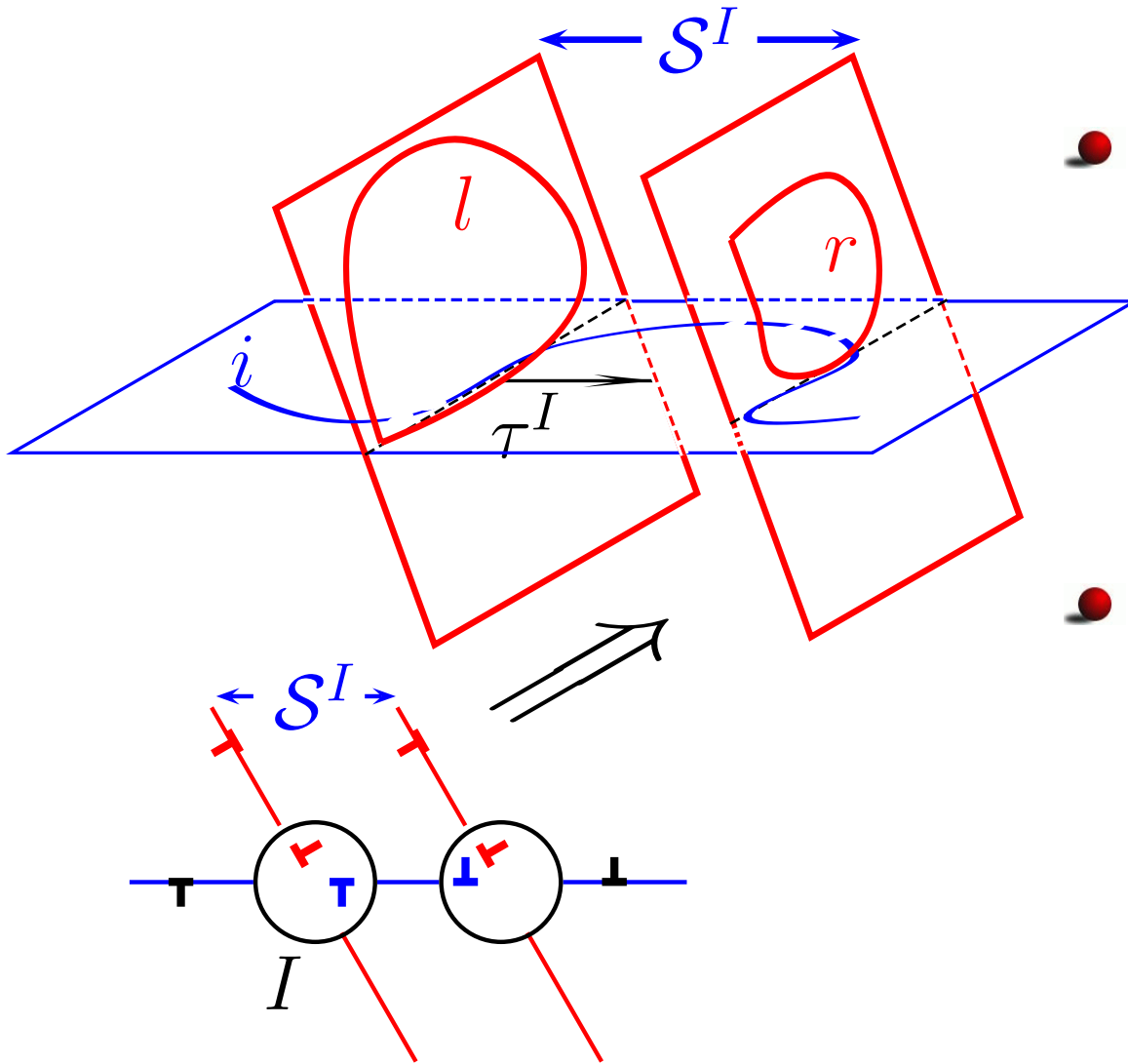
$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

● Critical Time

$$t_{\text{nuc}}^I = \underbrace{B\mathcal{F}(\xi)}_{\gamma} \frac{S^I}{|\tau^I| b^i}$$

$$10^{-4} < \gamma < 0.1$$

Dynamic Sources



● Critical Stress

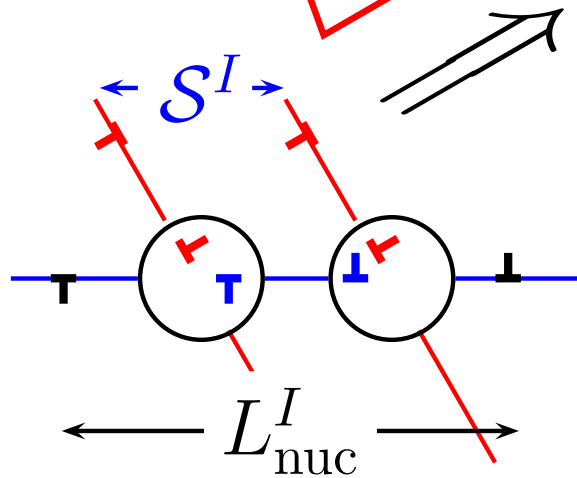
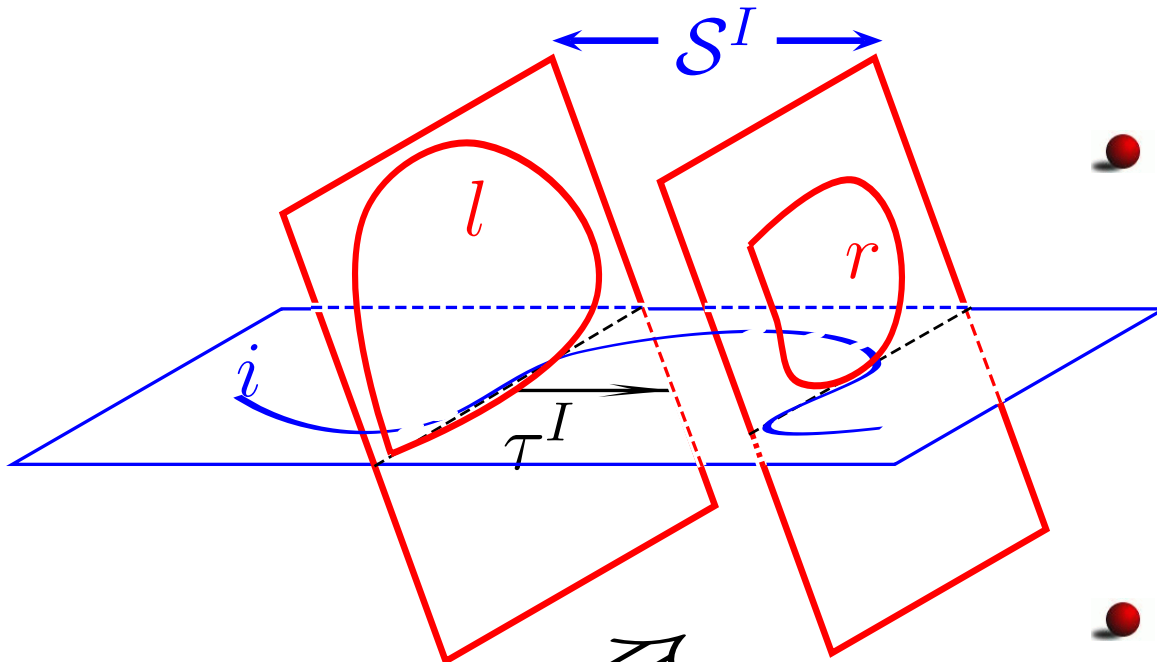
$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

● Critical Time

$$t_{\text{nuc}}^I = \underbrace{B\mathcal{F}(\xi)}_{\gamma} \frac{S^I}{|\tau^I| b^i}$$

$$10^{-4} < \gamma < 0.1$$

Dynamic Sources



- **Critical Stress**

$$\tau_{\text{nuc}}^I = \beta \frac{\mu b^i}{S^I}$$

- **Critical Time**

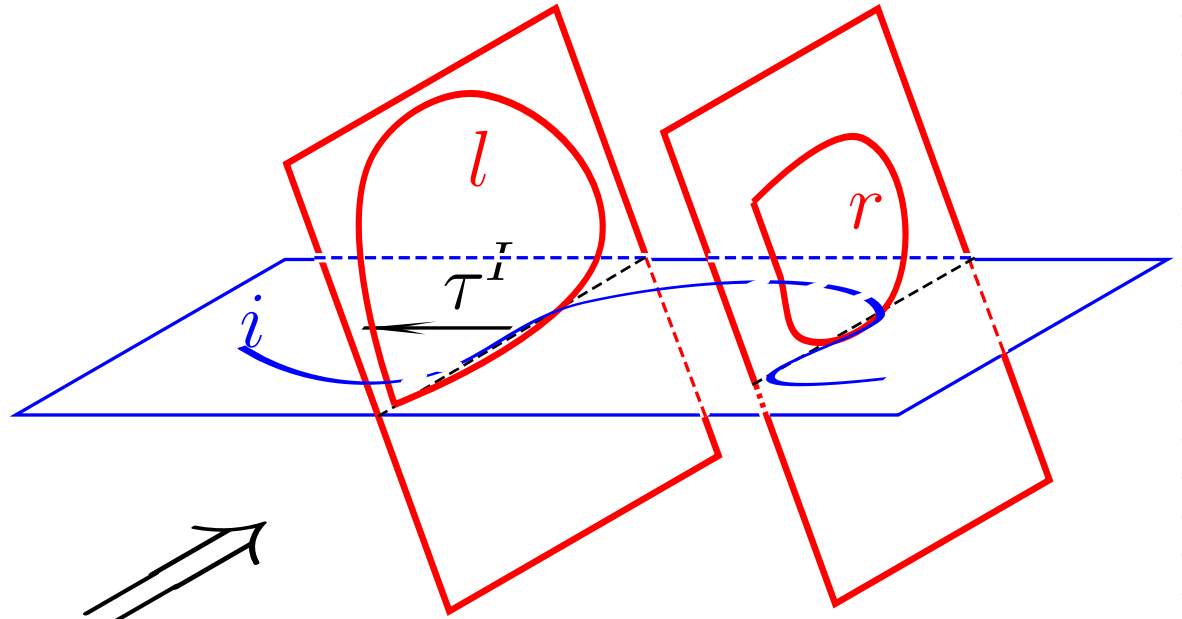
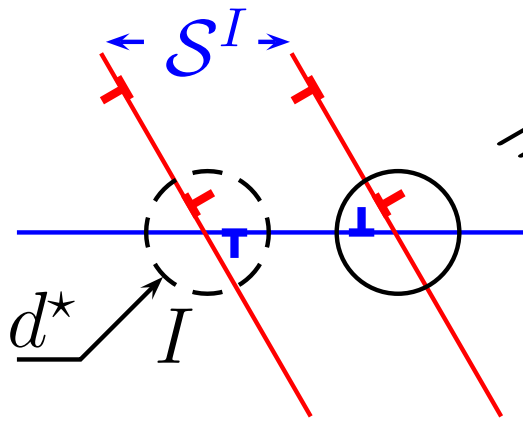
$$t_{\text{nuc}}^I = \underbrace{B\mathcal{F}(\xi)}_{\gamma} \frac{S^I}{|\tau^I| b^i}$$

$$10^{-4} < \gamma < 0.1$$

Dynamic Obstacles

- **Destruction rule**

$$\frac{f^I}{b^i} = \tau^I > \tau_{\text{brk}}^I$$

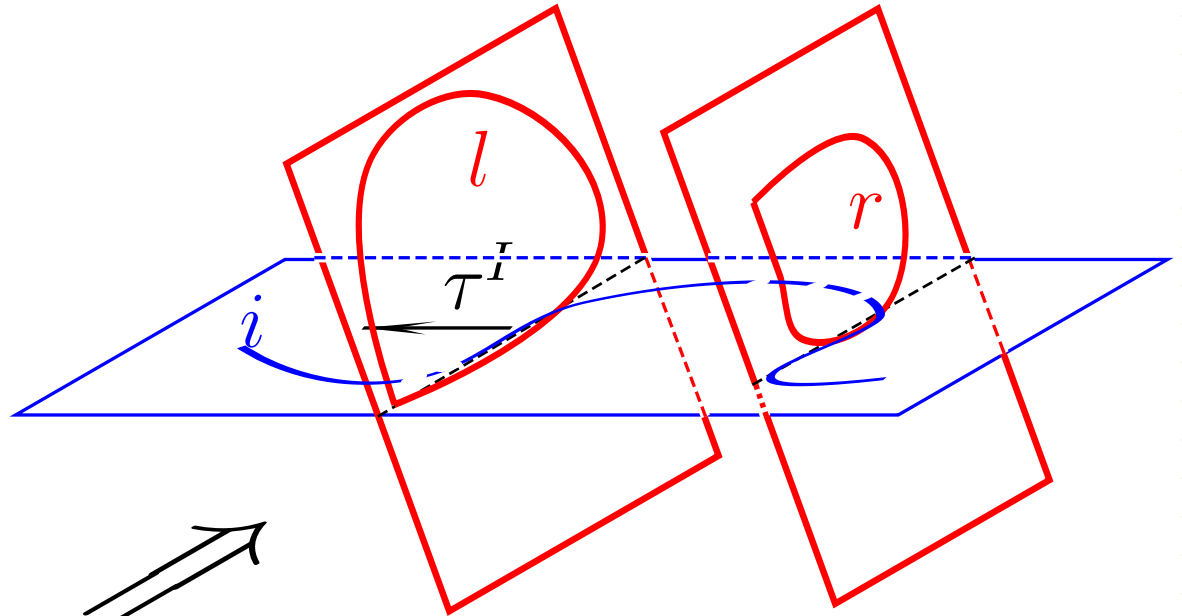
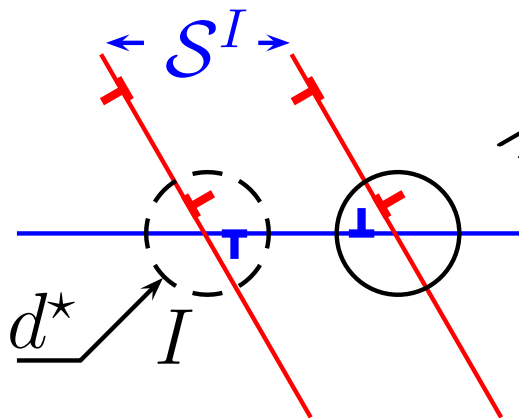


$\mathcal{S}^I \equiv$ nearest neighbor spacing (on either slip plane)

Dynamic Obstacles

- **Breaking Stress**

$$\tau_{\text{brk}}^I \equiv \beta \mu \frac{b^i}{S^I}$$



$S^I \equiv$ nearest neighbor spacing (on either slip plane)



Interaction junction/dislocation

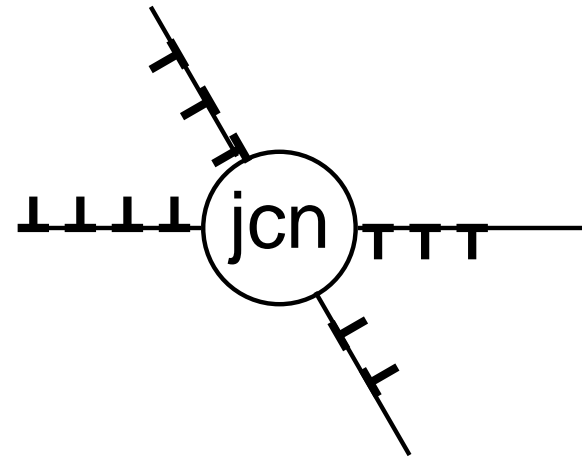
- Obstacles are not destroyed by annihilation



Interaction junction/dislocation

- Obstacles are not destroyed by annihilation

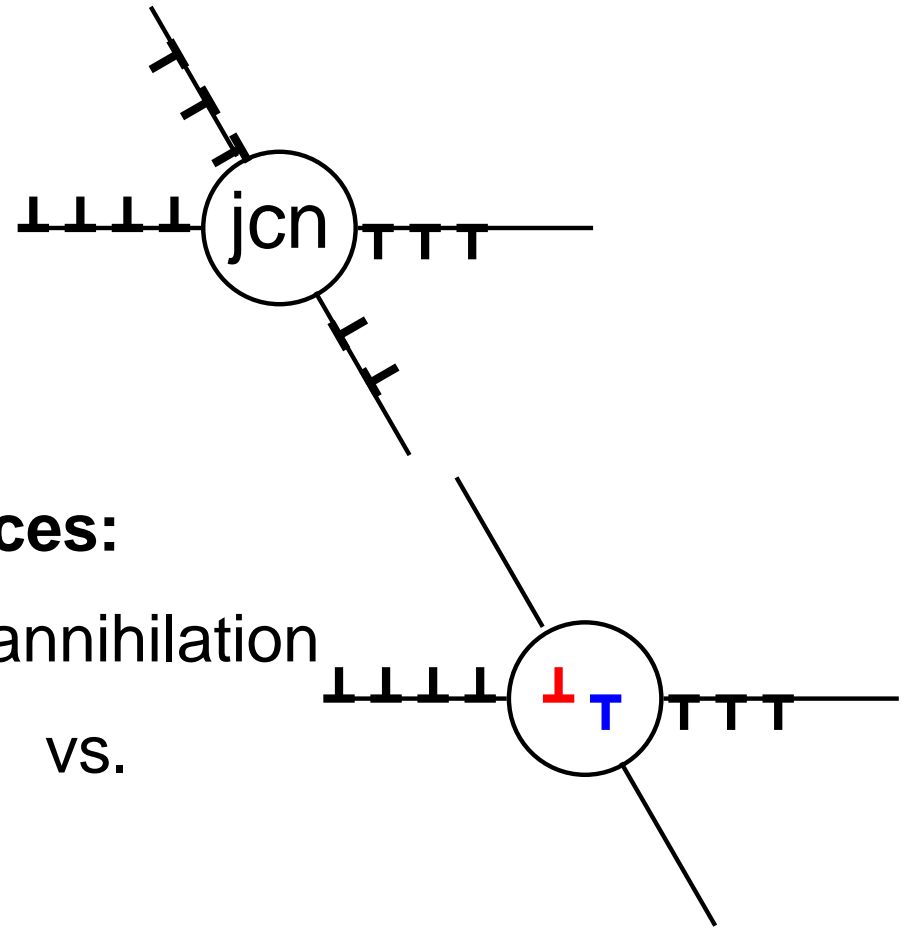
- **Pinning at obstacles:**



Interaction junction/dislocation

- Obstacles are not destroyed by annihilation

- **Pinning at obstacles:**



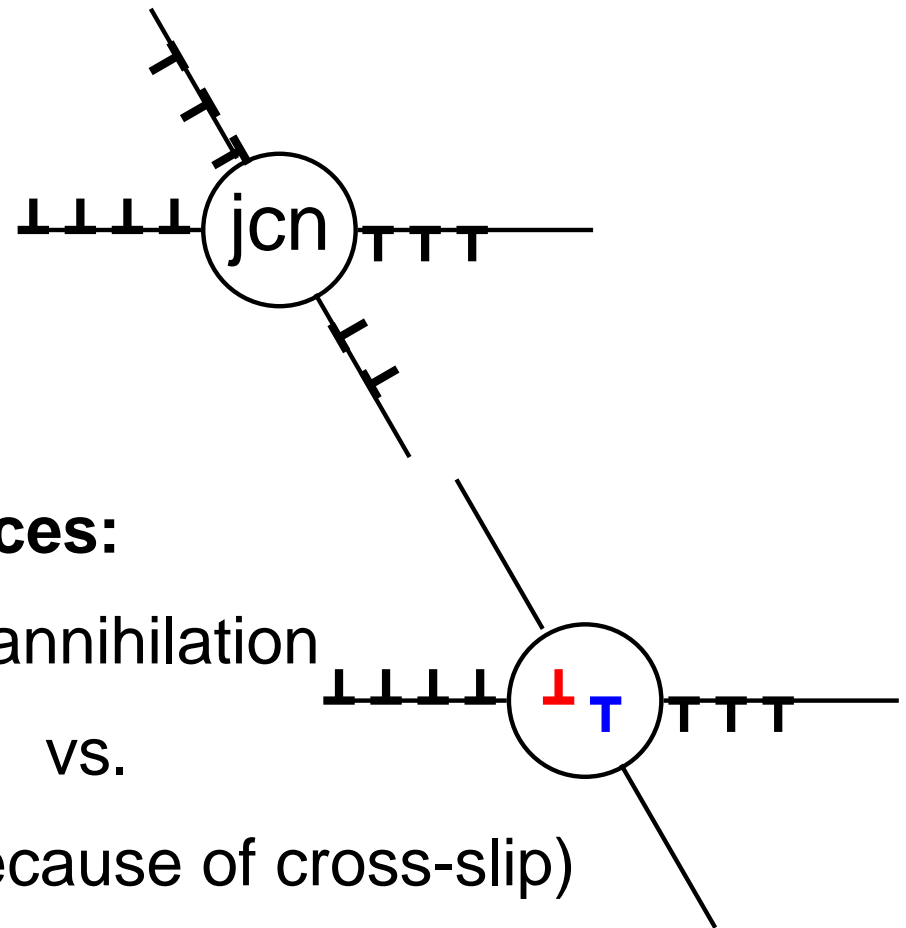
- **Special behavior of sources:**

- Rule of destruction by annihilation

Interaction junction/dislocation

- Obstacles are not destroyed by annihilation

- **Pinning at obstacles:**



- **Special behavior of sources:**

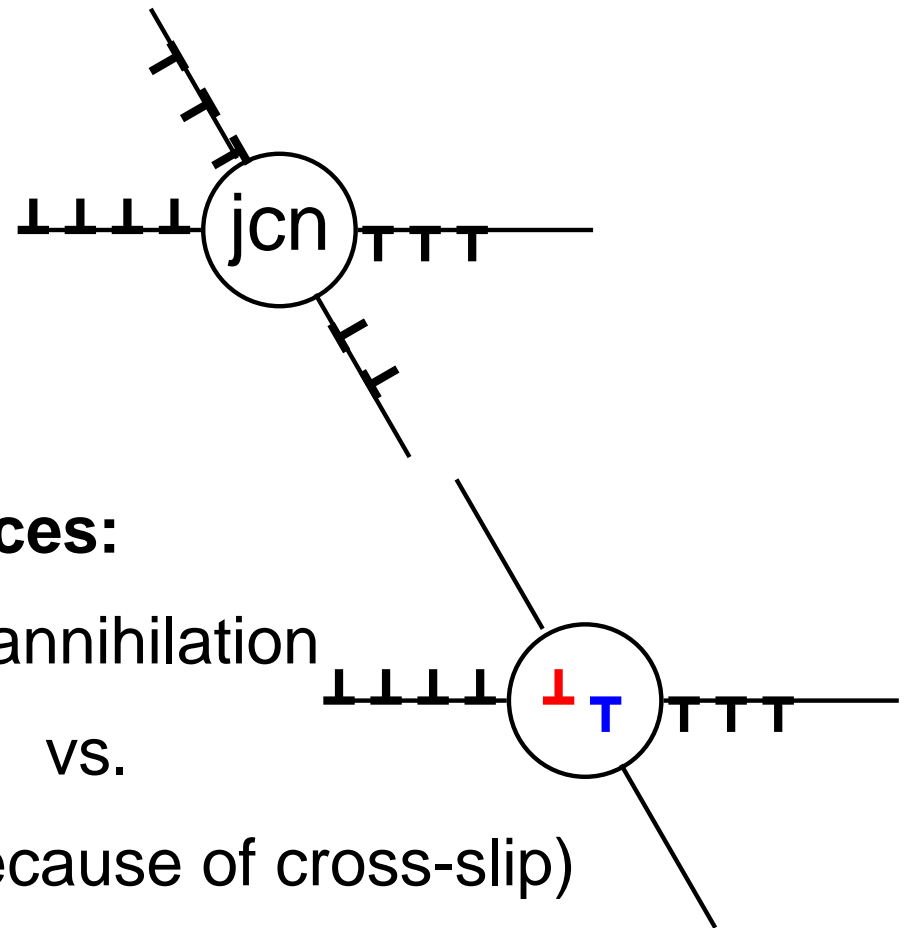
- Rule of destruction by annihilation

- Transparent source (because of cross-slip)

Interaction junction/dislocation

- Obstacles are not destroyed by annihilation

- **Pinning at obstacles:**



- **Special behavior of sources:**

- Rule of destruction by annihilation

- Transparent source (because of cross-slip)



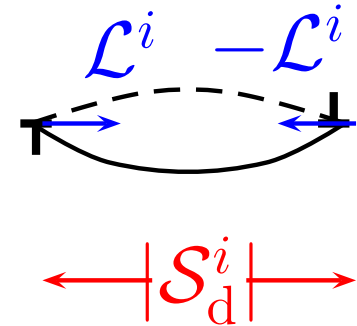
Annihilation & Line Tension

- **Annihilation:** critical distance L_e

Annihilation & Line Tension

- **Annihilation:** critical distance L_e
- **Line tension:**

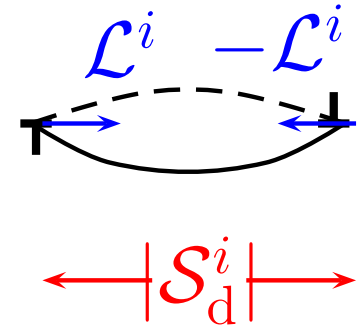
$$\mathcal{L}^i = -\alpha \frac{\mu |b^i|}{S_d^i}$$



Annihilation & Line Tension

- **Annihilation:** critical distance L_e
- **Line tension:**

$$\mathcal{L}^i = -\alpha \frac{\mu |b^i|}{S_d^i}$$

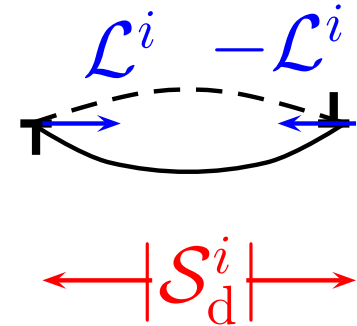


- **Change of partner:**

Annihilation & Line Tension

- **Annihilation:** critical distance L_e
- **Line tension:**

$$\mathcal{L}^i = -\alpha \frac{\mu |b^i|}{S_d^i}$$



- **Change of partner:**
 - *after annihilation*

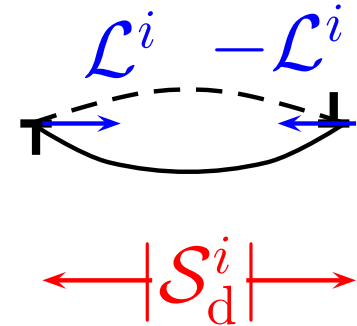


Annihilation & Line Tension

- Annihilation: critical distance L_e

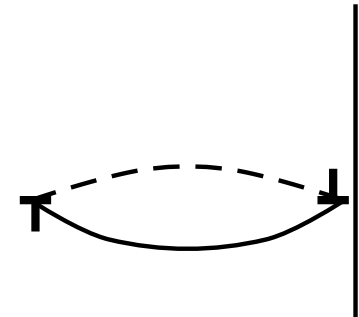
- Line tension:

$$\mathcal{L}^i = -\alpha \frac{\mu |b^i|}{S_d^i}$$



- Change of partner:

- *after annihilation*
- *exiting at free surface*





Dislocation Glide

Viscous drag generalized into:

$$Bv^i = (\tau^i - \tau_P + \mathcal{L}^i) b^i$$

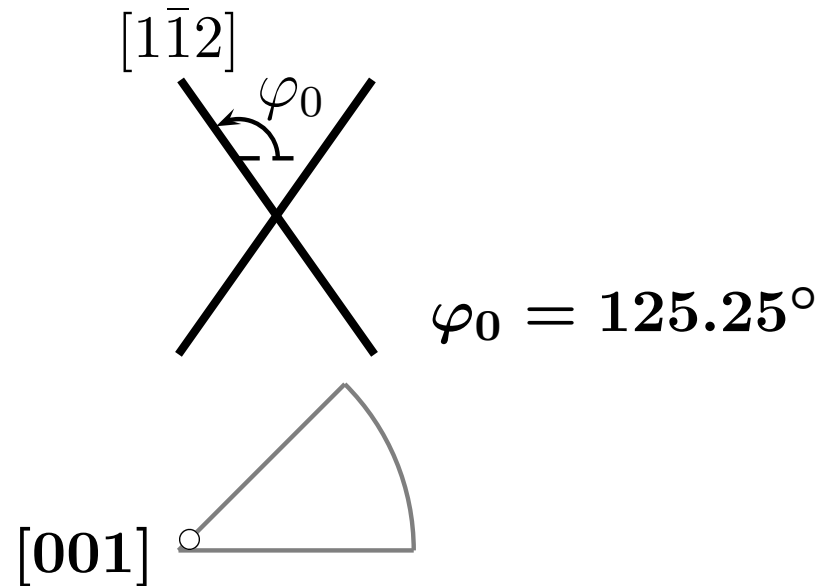
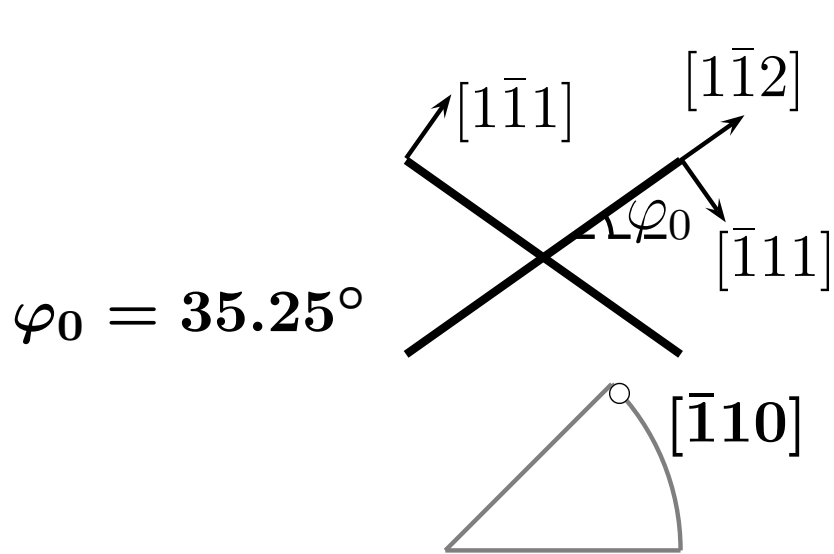
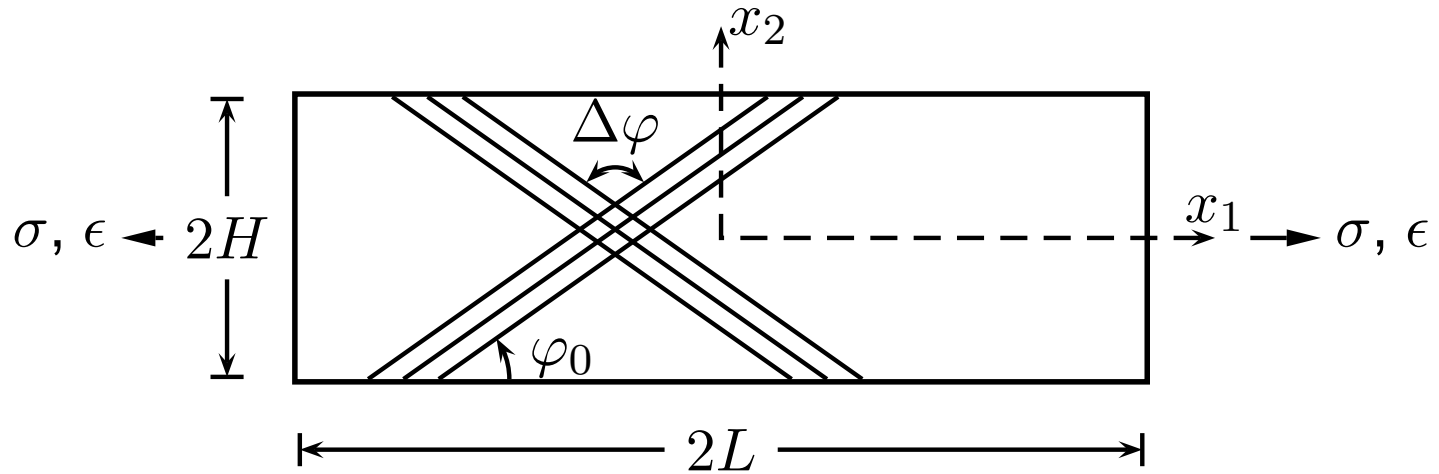




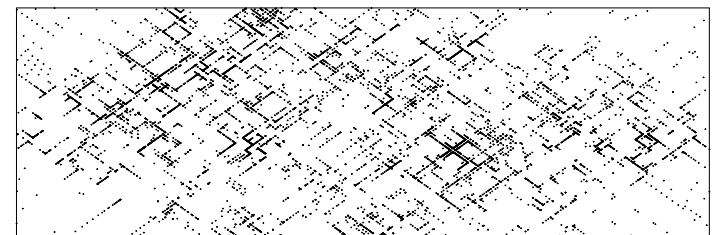
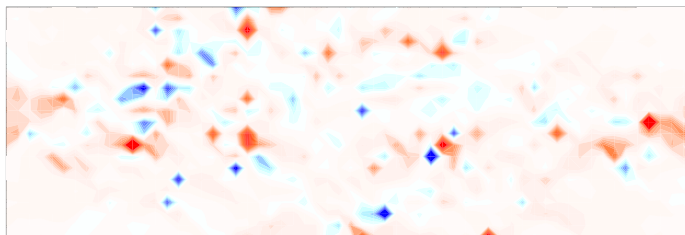
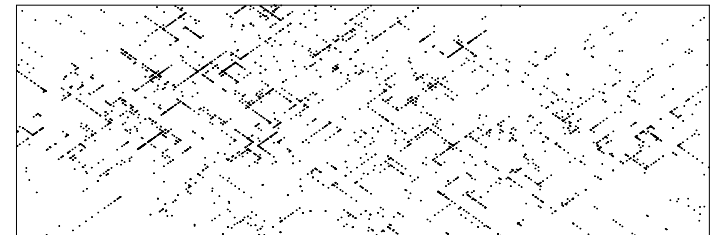
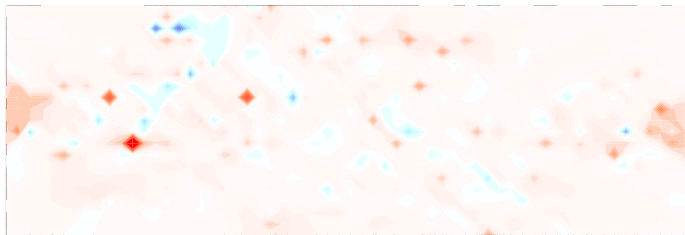
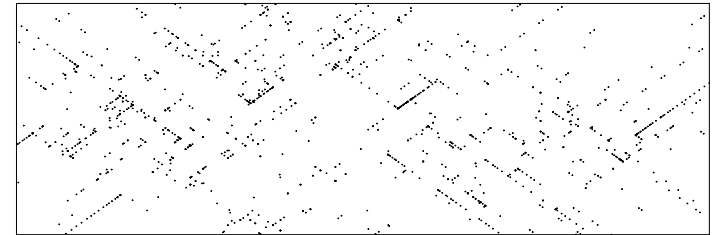
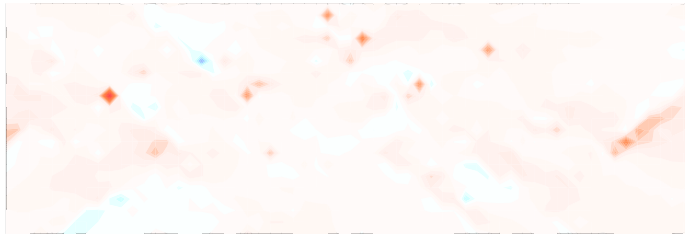
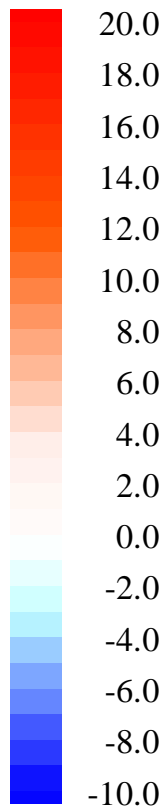
Outline

1. Discrete Dislocation Plasticity
2. 3D Rules in 2D Framework
3. **Work-Hardening (isotropic? dissipative?)**
4. Relation to geometric hardening and GNDs
5. The Stored Energy of Cold Work

Work-Hardening



Phenomenology



1 μm

stress σ_{11}/σ

pattern



Two-Stage Hardening

- slip plane spacing $d = 50b$
- static sources with $\rho_0 = 4.9 \times 10^{13} \text{ m}^{-2}$
- **initially non-symmetric glide**
- **crystal size: $6 \mu\text{m} \times 2 \mu\text{m}$**

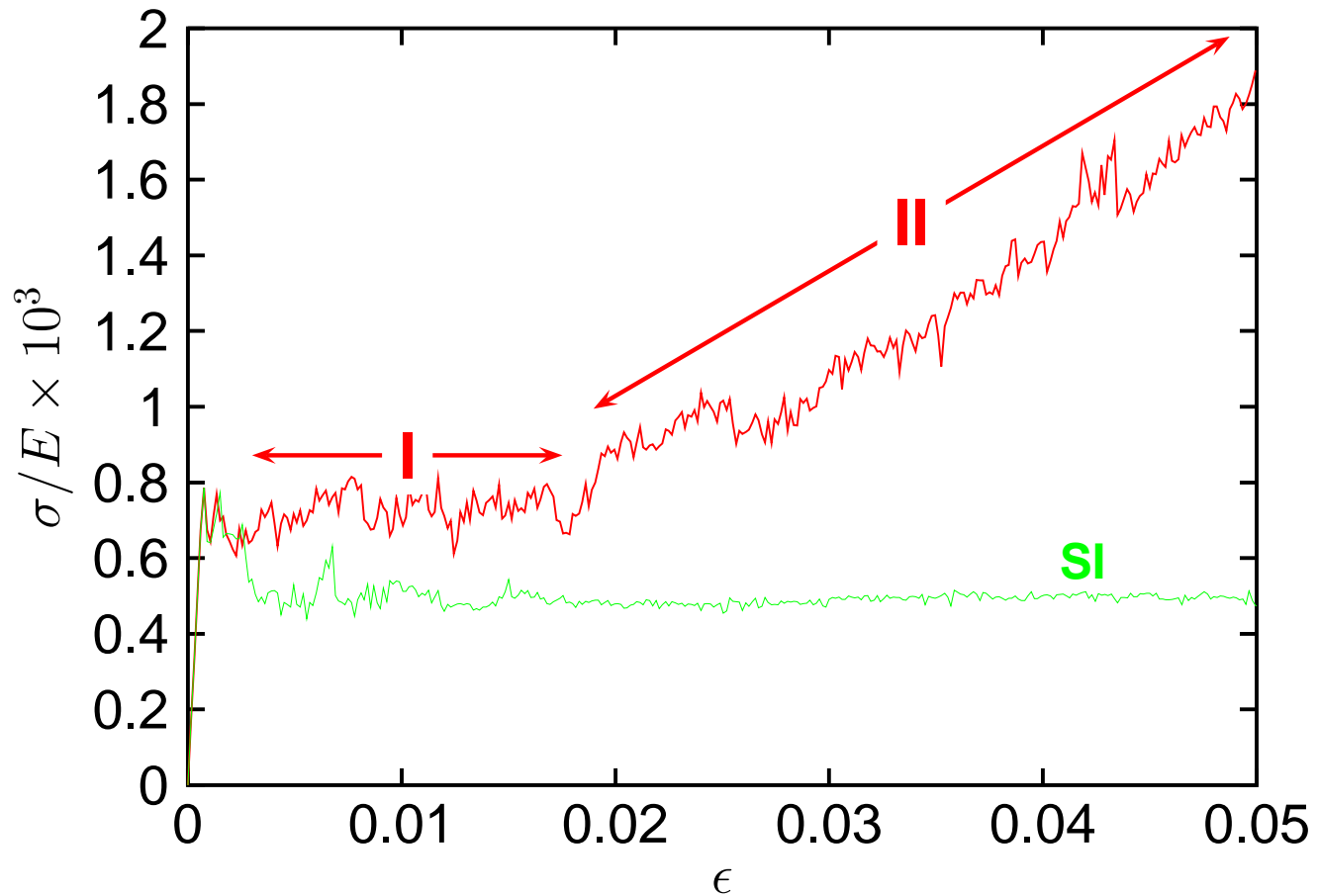


Two-Stage Hardening

- slip plane spacing $d = 50b$
- static sources with $\rho_0 = 4.9 \times 10^{13} \text{ m}^{-2}$
- **initially non-symmetric glide**
- **crystal size:** $6 \mu\text{m} \times 2 \mu\text{m}$
- **parameters for 3D rules:**
 - *critical junction distance* $d^* = 6b$
 - *formation probability of anchoring points* $p = 0.05$
 - *breaking stress parameter* $\beta = 1$
 - *nucleation time parameter* $\gamma = 0.1$
 - *line tension coefficient* $\alpha = 0$



Two-Stage Hardening





Comparison with experiments

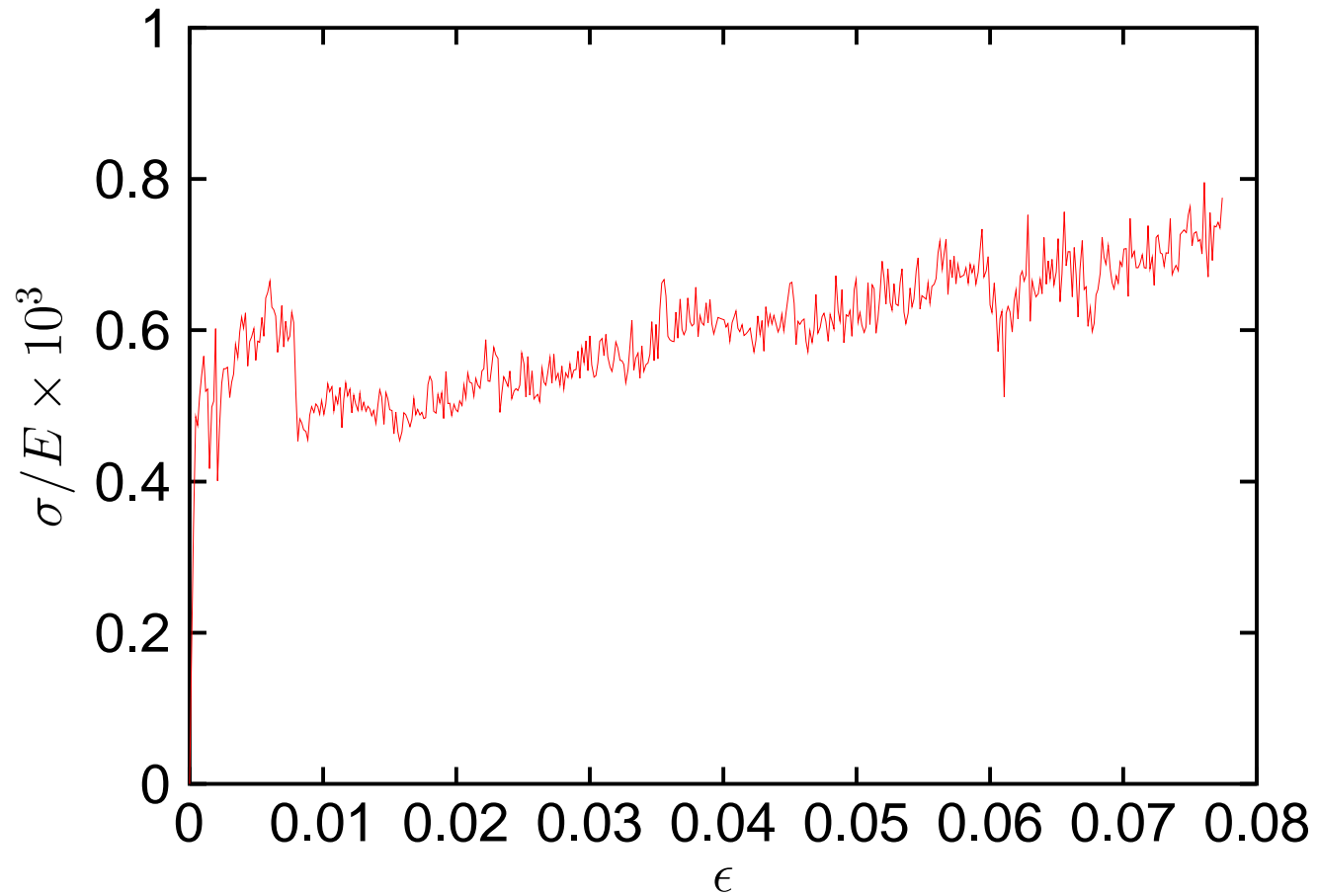
- slip plane spacing $d = 25b$
- static sources with $\rho_0 = 9.7 \times 10^{13} \text{ m}^{-2}$
- **parameters for 3D rules:**
 - *formation probability of anchoring points* $p = 0.02$
 - *breaking stress parameter* $\beta = 5$



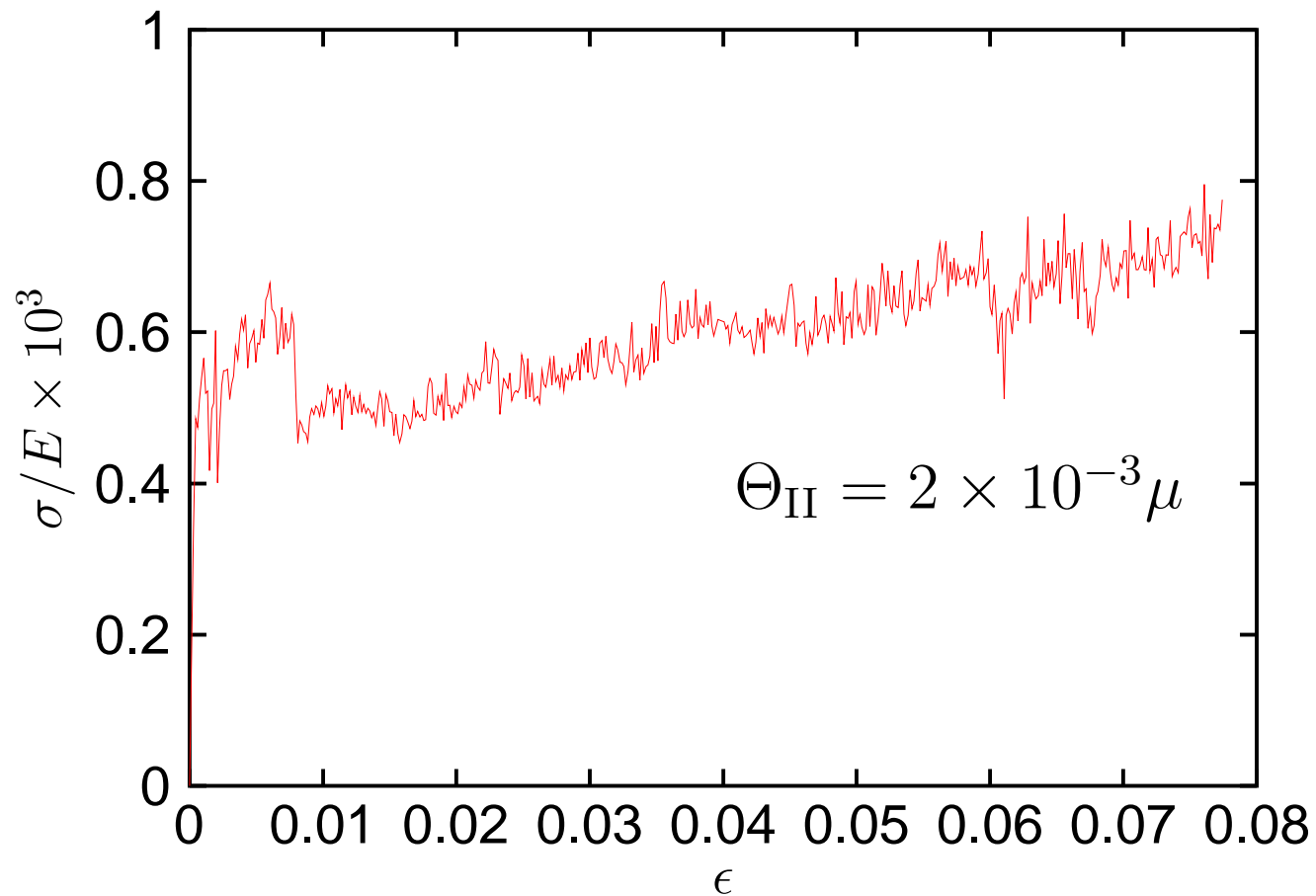
Comparison with experiments

- slip plane spacing $d = 25b$
- static sources with $\rho_0 = 9.7 \times 10^{13} \text{ m}^{-2}$
- **parameters for 3D rules:**
 - *formation probability of anchoring points* $p = 0.02$
 - *breaking stress parameter* $\beta = 5$
- Sources can be destroyed by annihilation

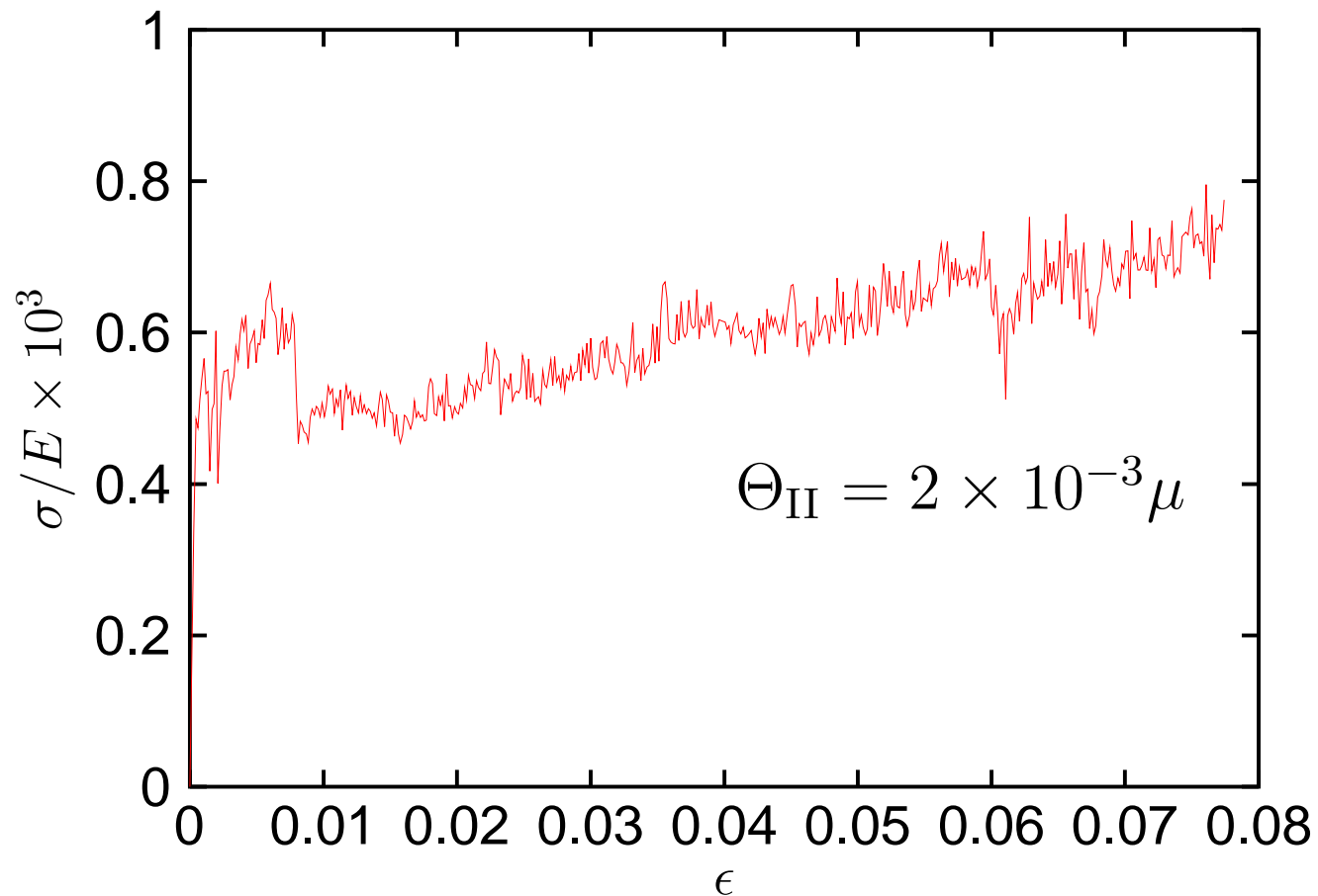
Comparison with experiments



Comparison with experiments

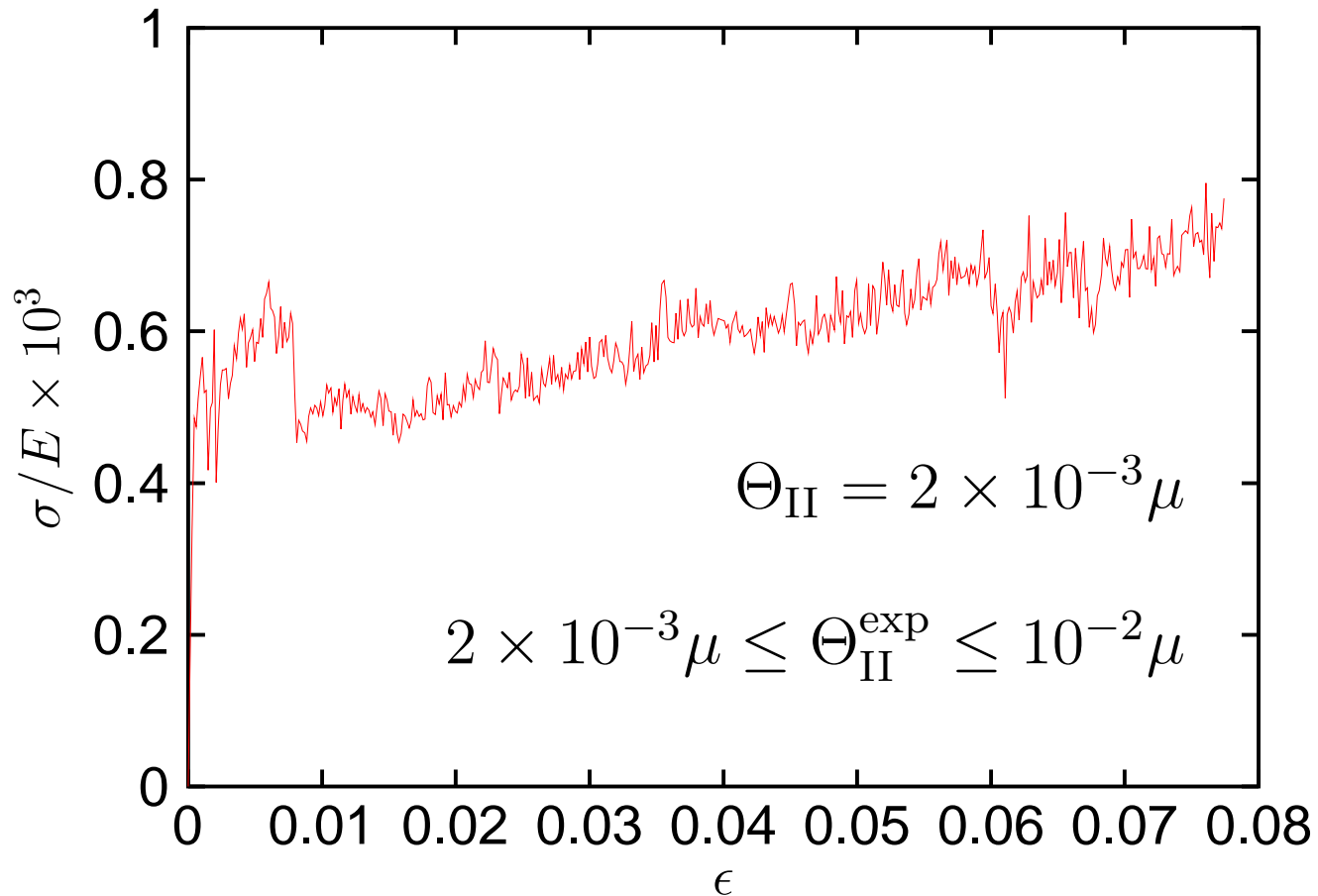


Comparison with experiments



Sources can be destroyed by annihilation

Comparison with experiments



Sources can be destroyed by annihilation

Flow Stress

With $\mathcal{T} = \sigma f_s = \sigma (1/2 \sin(2\varphi_0))$

For stage II

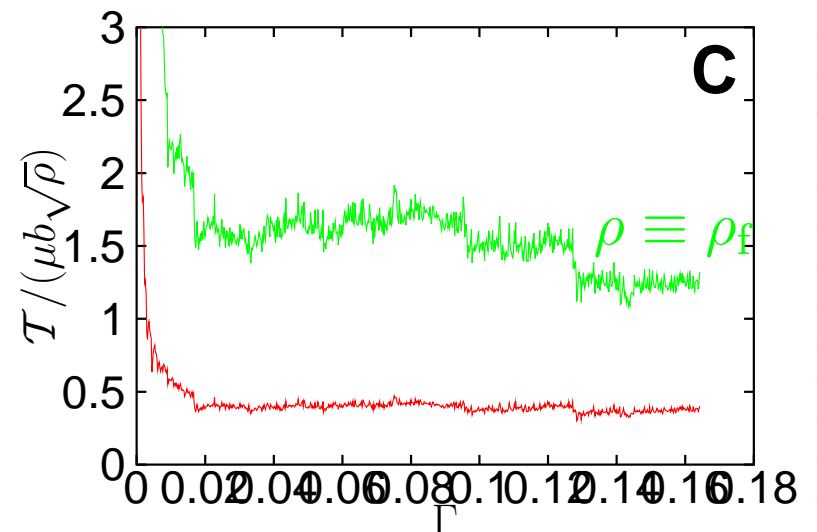
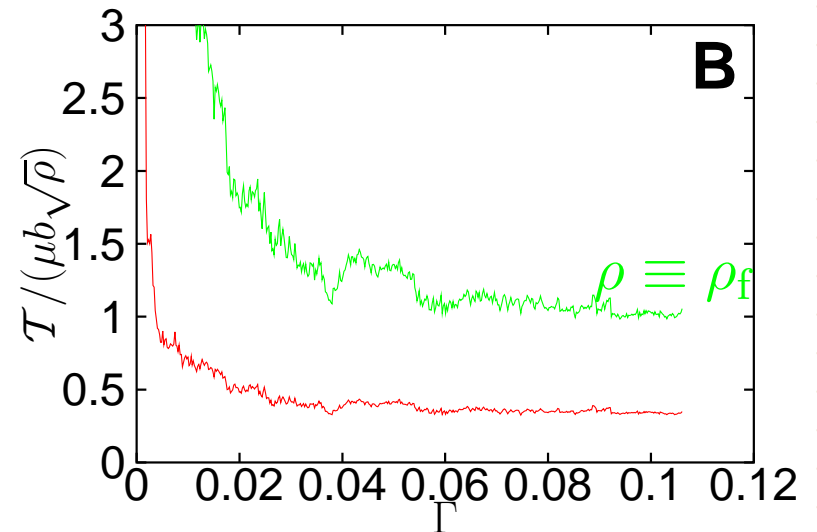
$$\mathcal{T}/\mu = A \times b \times \sqrt{\rho}$$

$$\mathcal{T}/\mu = A^f \times b \times \sqrt{\rho_f}$$

Averaging over several runs:

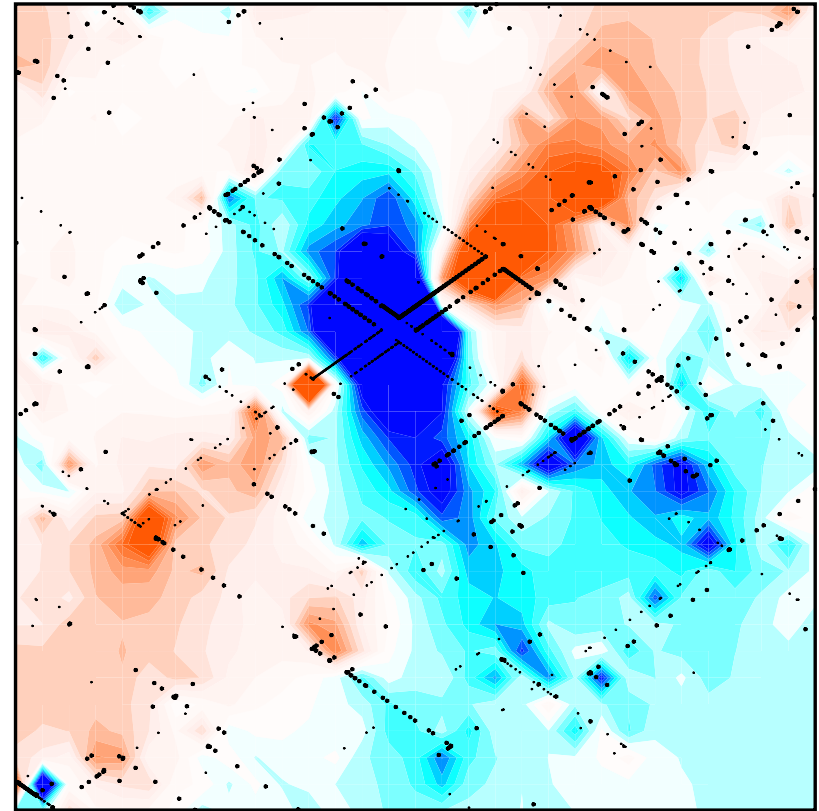
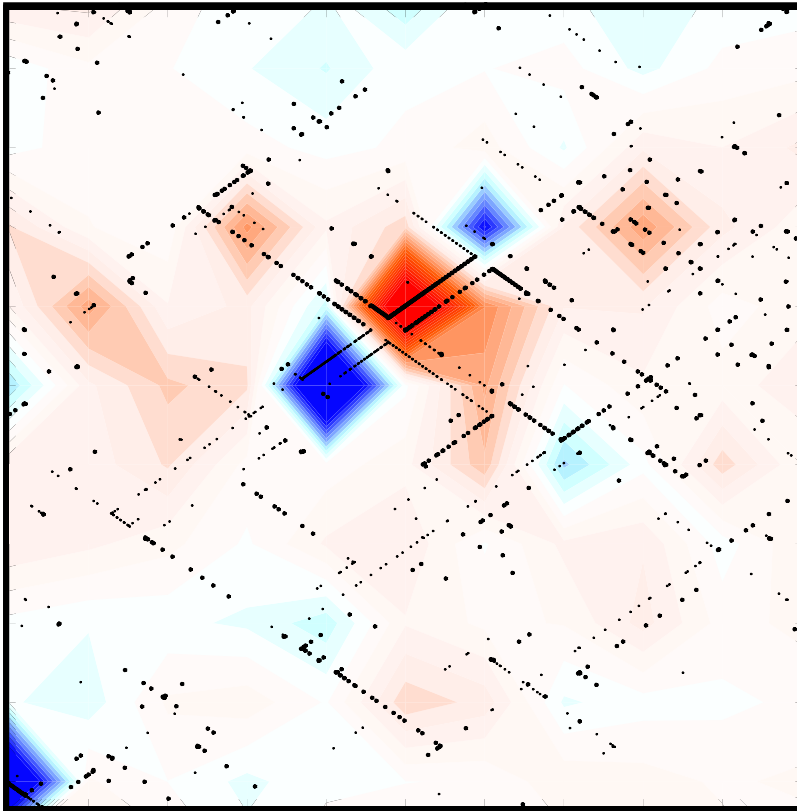
● $0.4 \leq A \leq 0.5$

● $1.0 \leq A^f \leq 1.8$



Cell Formation

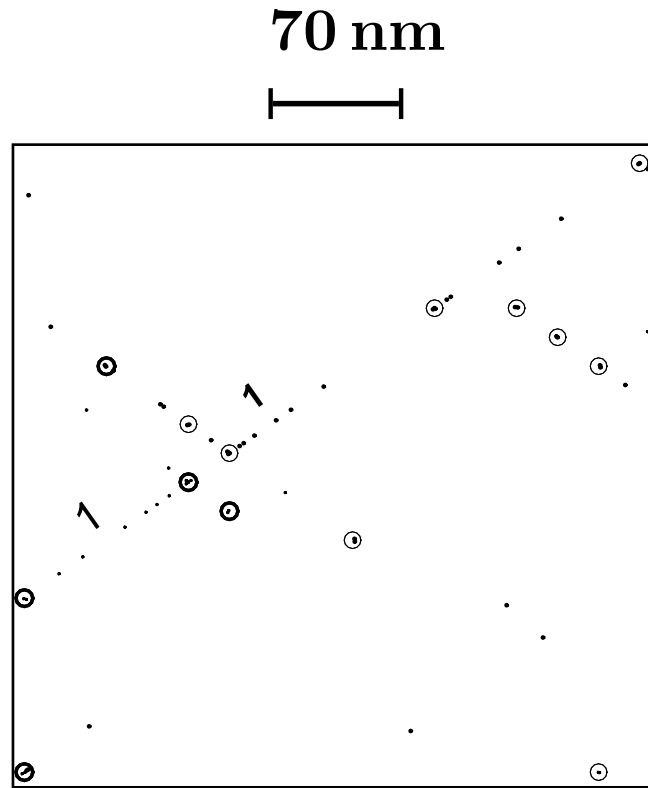
250 nm



Superposed σ_{11}/σ -field

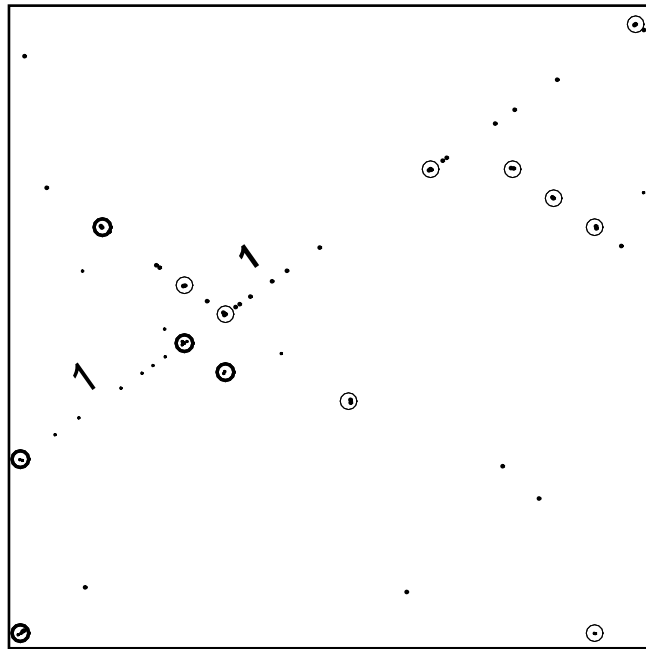
Superposed θ -field

Structure of Incipient Cell



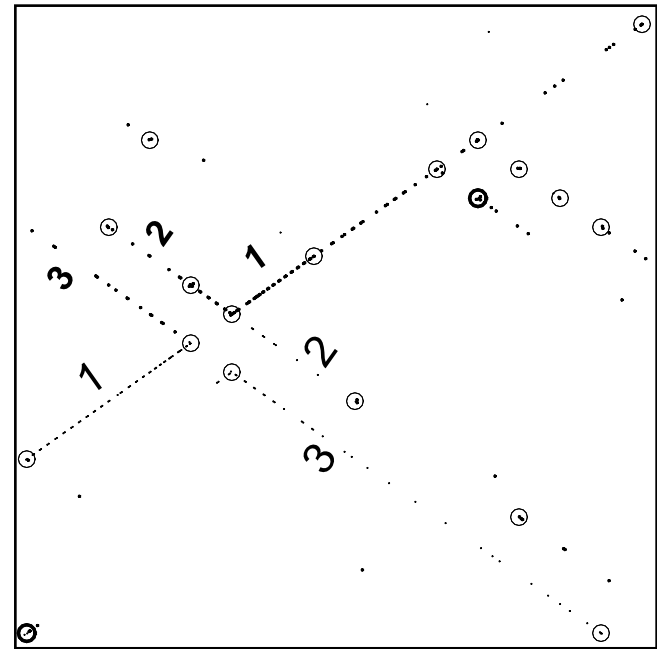
Structure of Incipient Cell

70 nm



$\epsilon = 0.020$

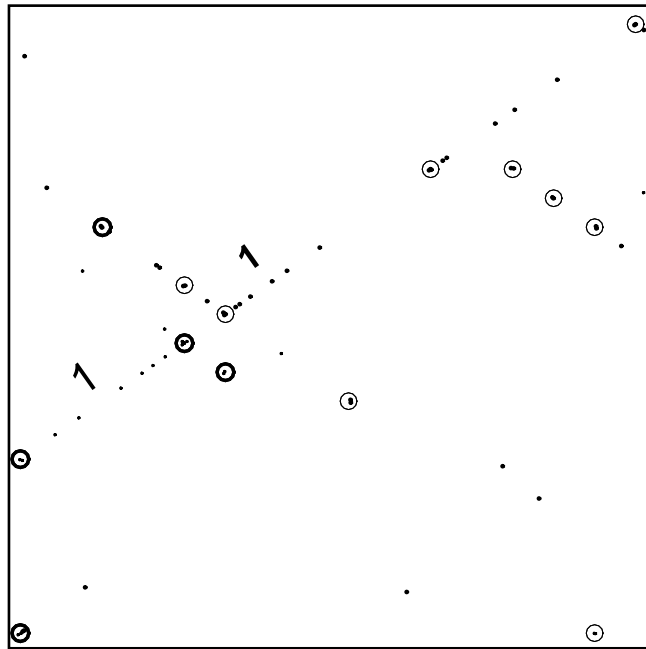
70 nm



$\epsilon = 0.025$

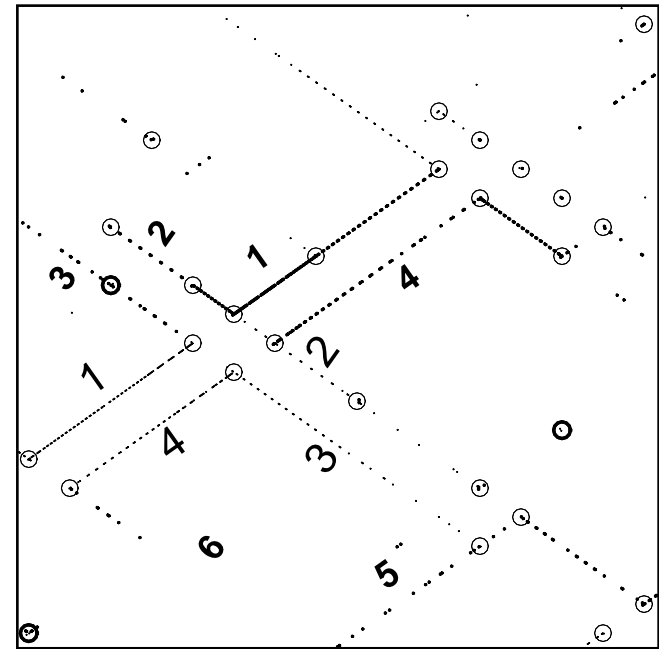
Structure of Incipient Cell

70 nm



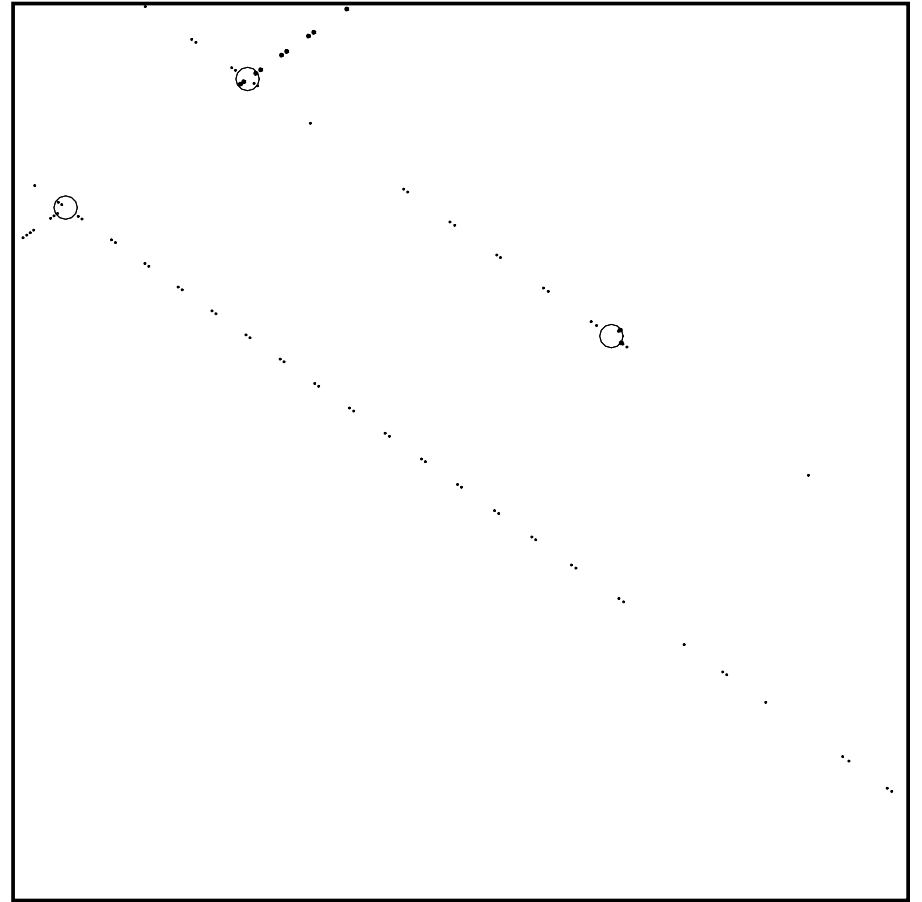
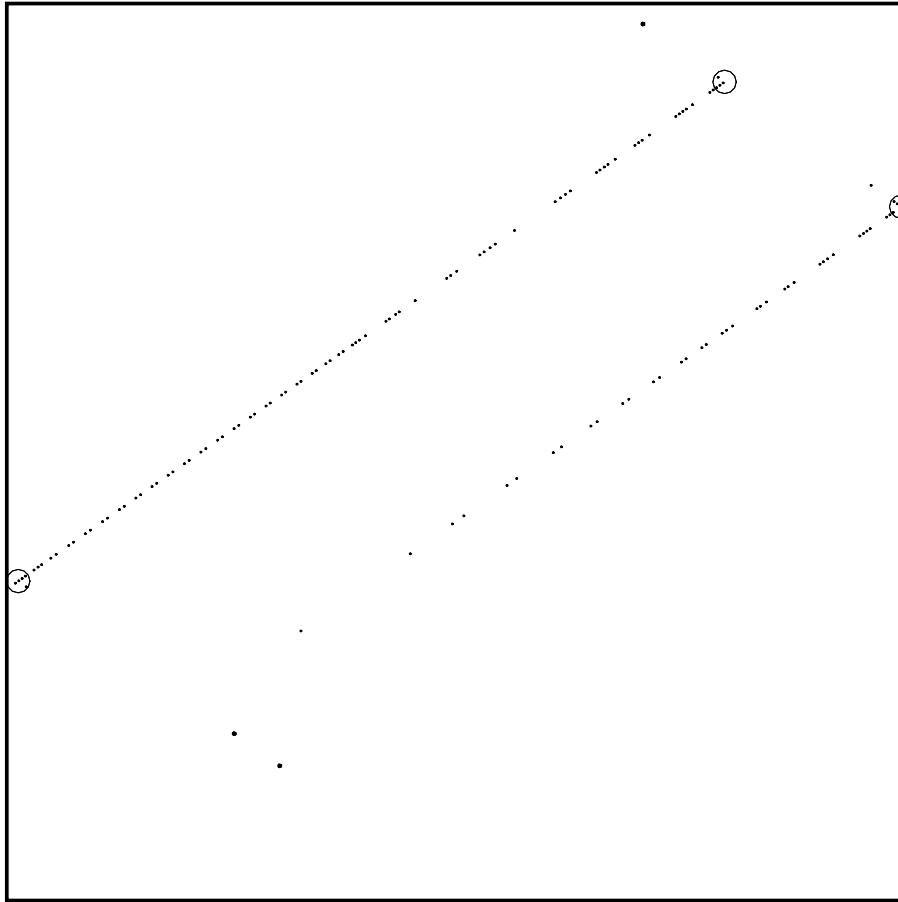
$\epsilon = 0.020$

70 nm



$\epsilon = 0.035$

Fine Wall Structure



10 nm

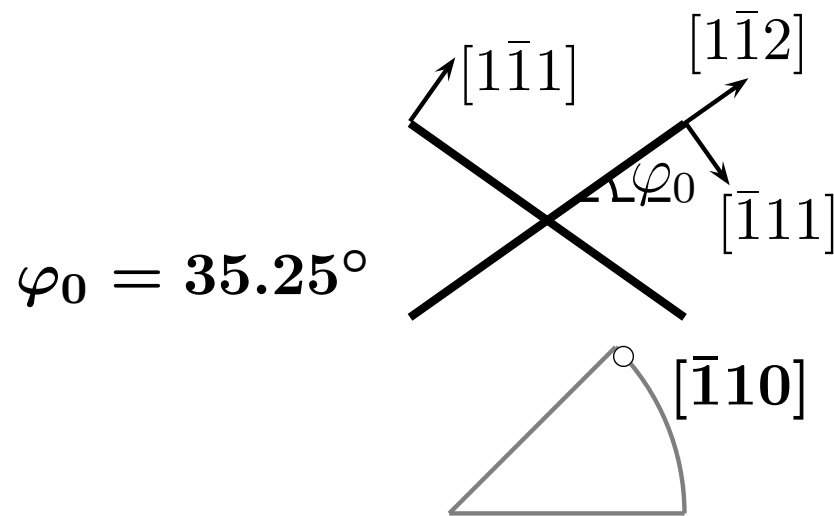
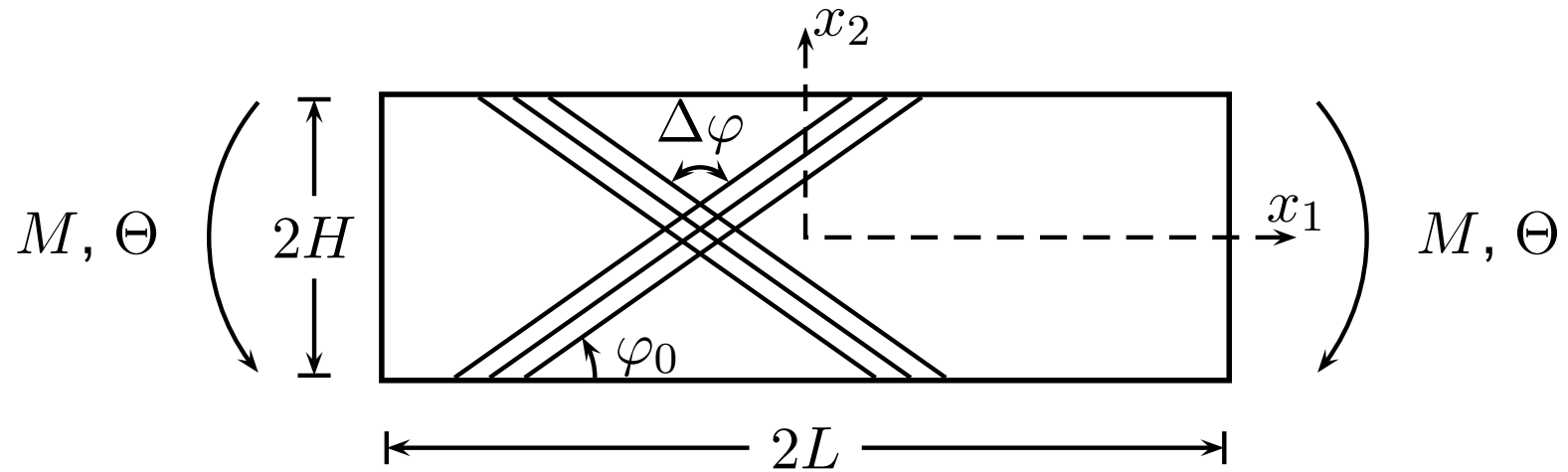




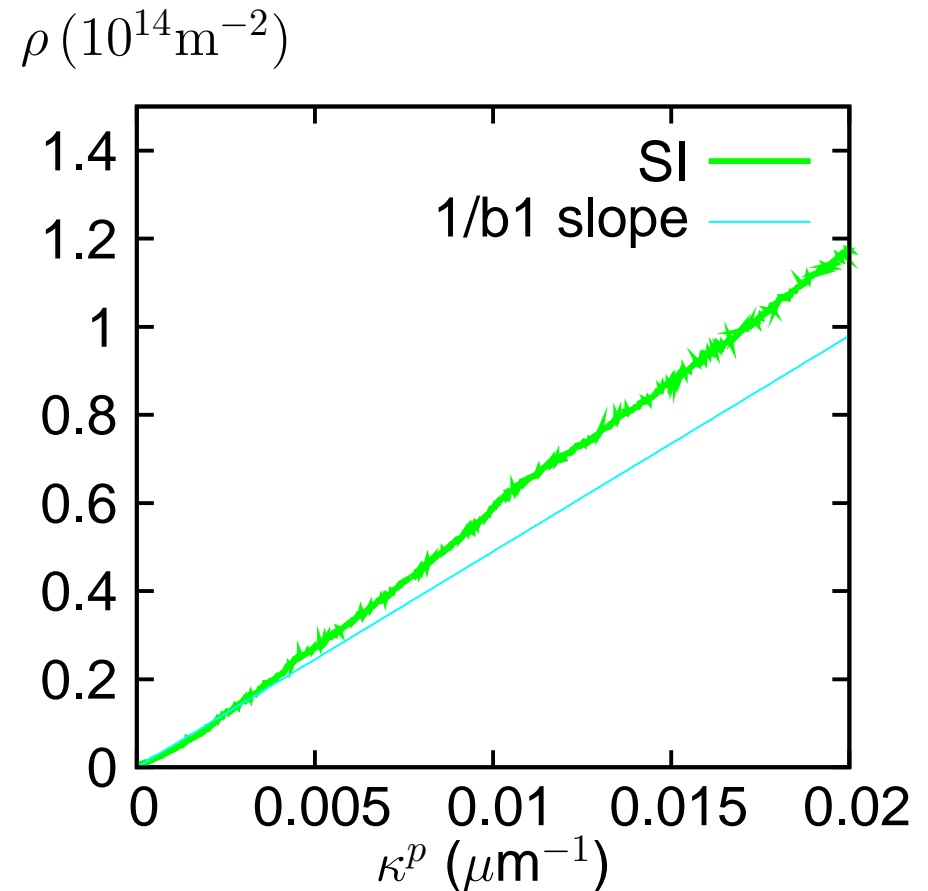
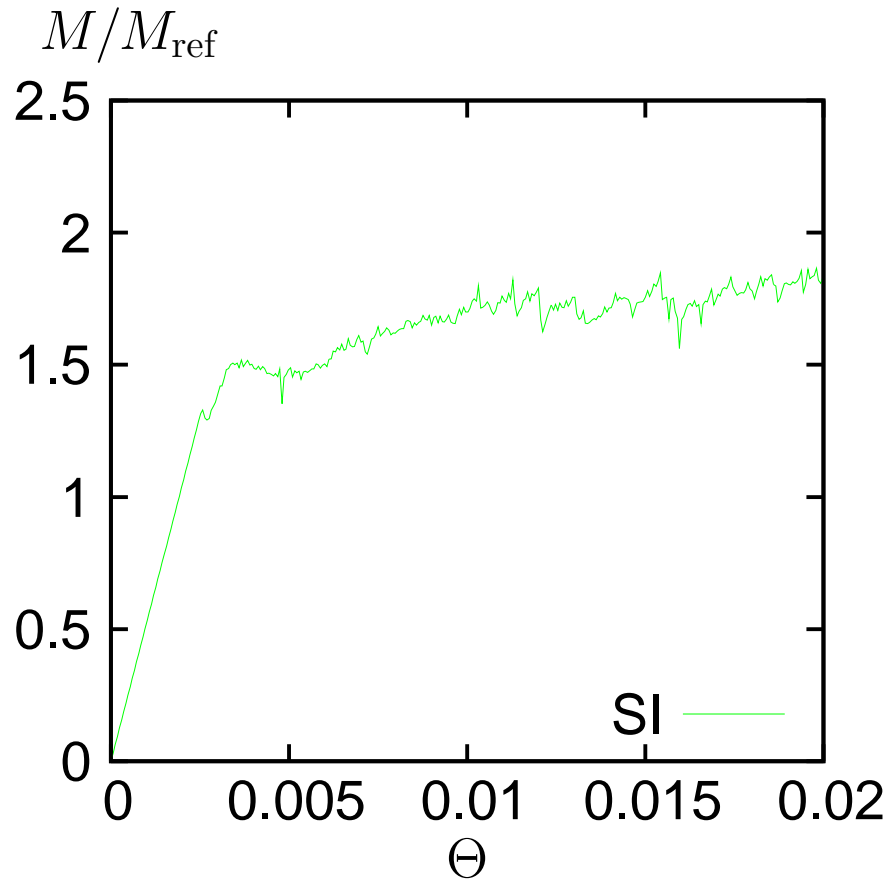
Outline

1. Discrete Dislocation Plasticity
2. 3D Rules in 2D Framework
3. Work-Hardening
4. **Relation to geometric hardening and GNDs**
5. The Stored Energy of Cold Work

Bending



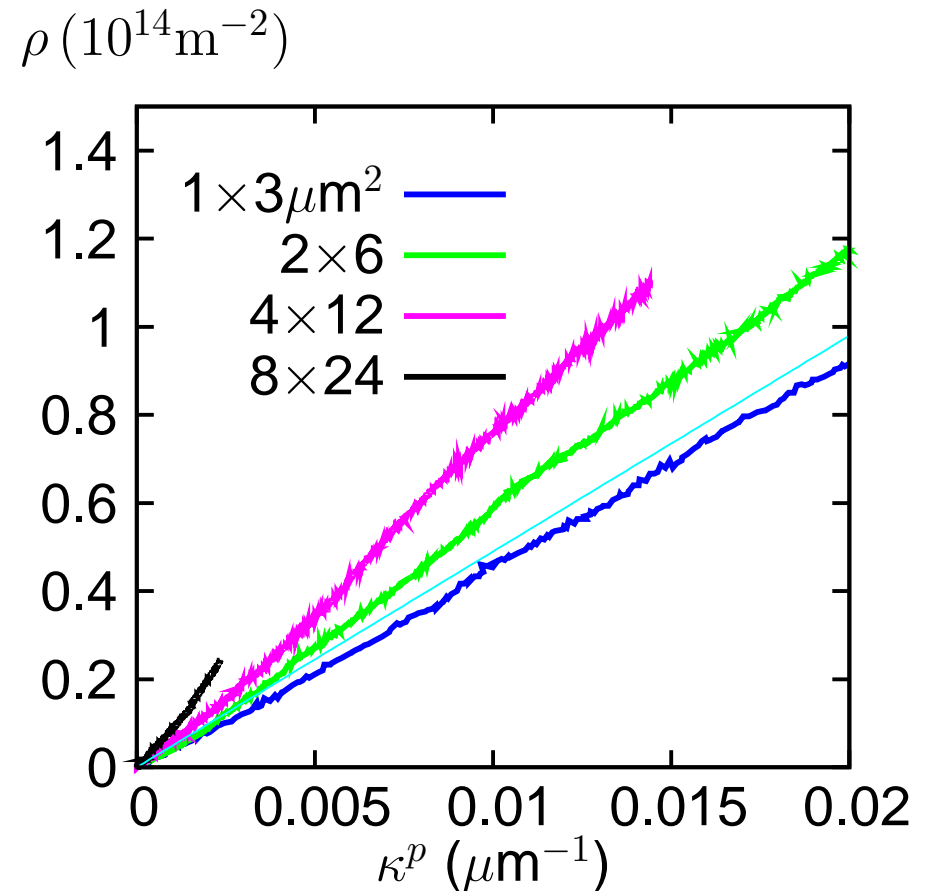
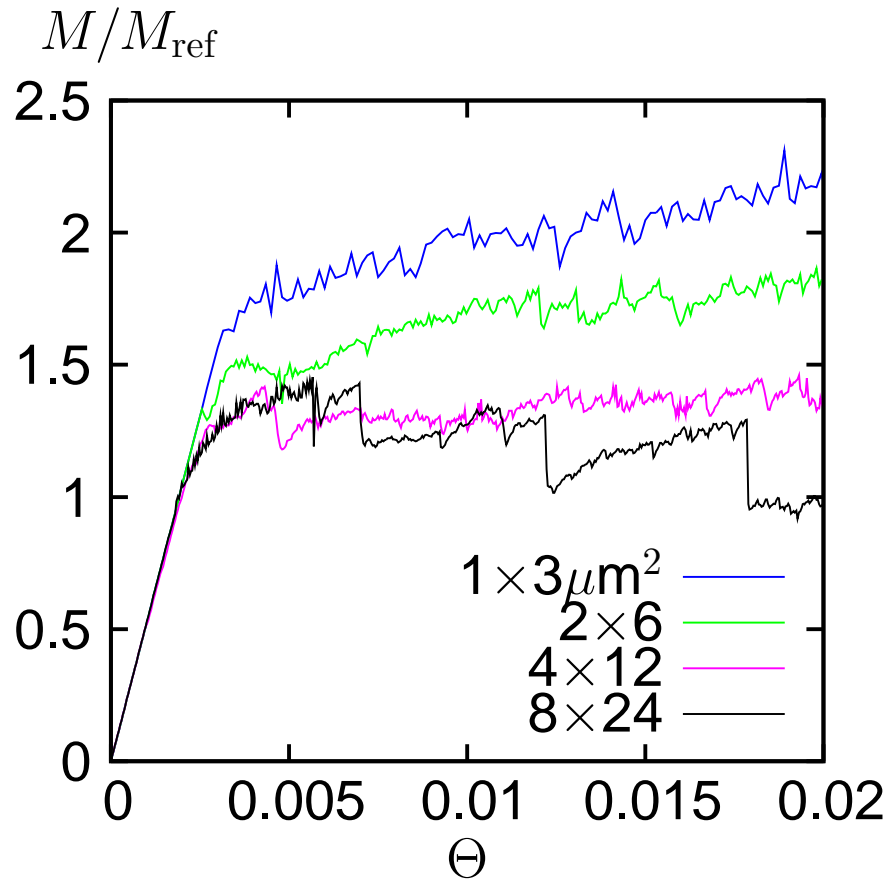
Bending (2D rules)



$$M = \int_R \sigma_{11} x_2 dx_2$$

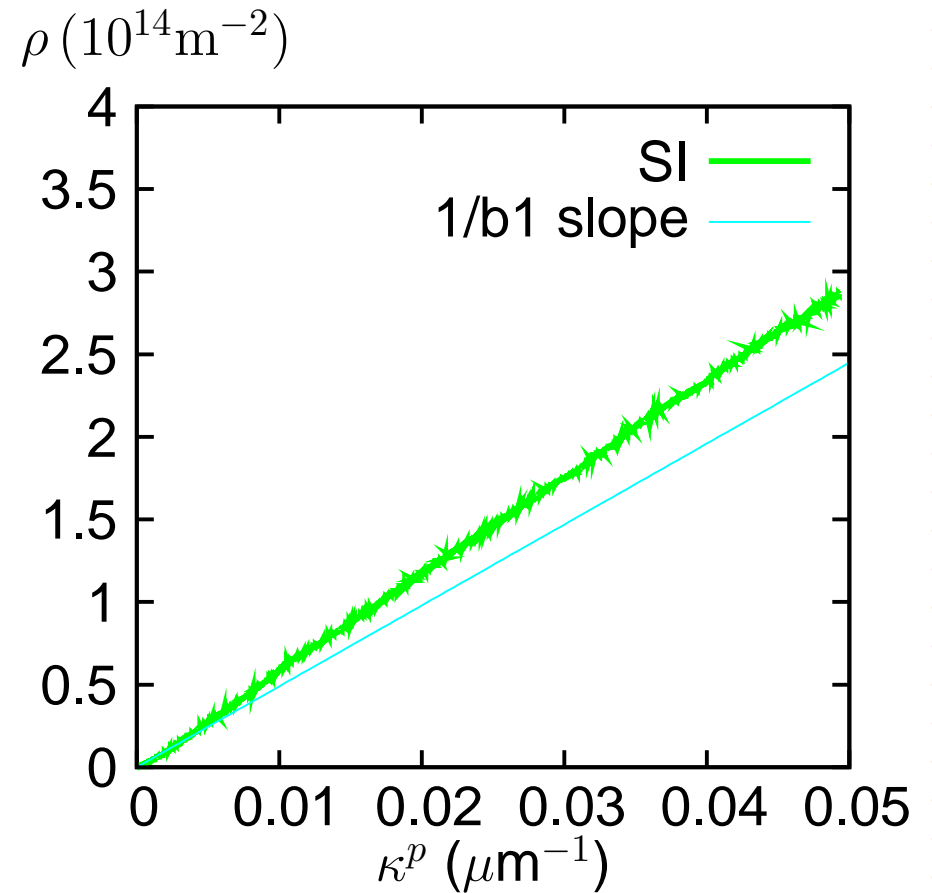
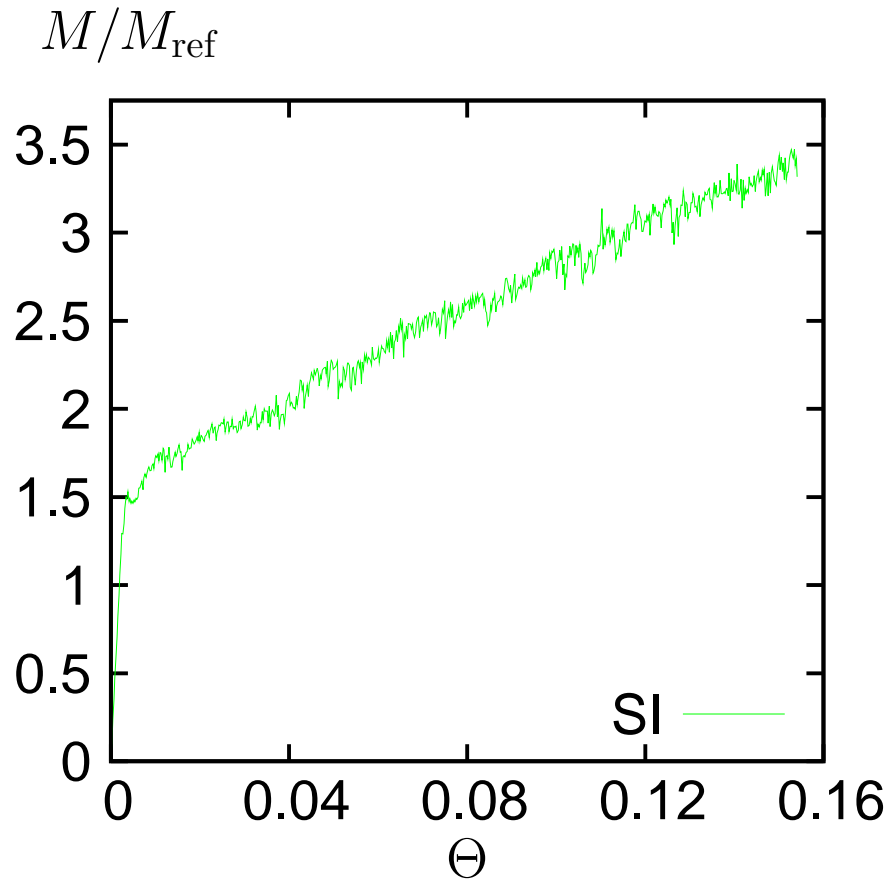
$$\kappa^p = \frac{\Theta}{L} - \frac{M}{D}$$

Bending (2D rules)

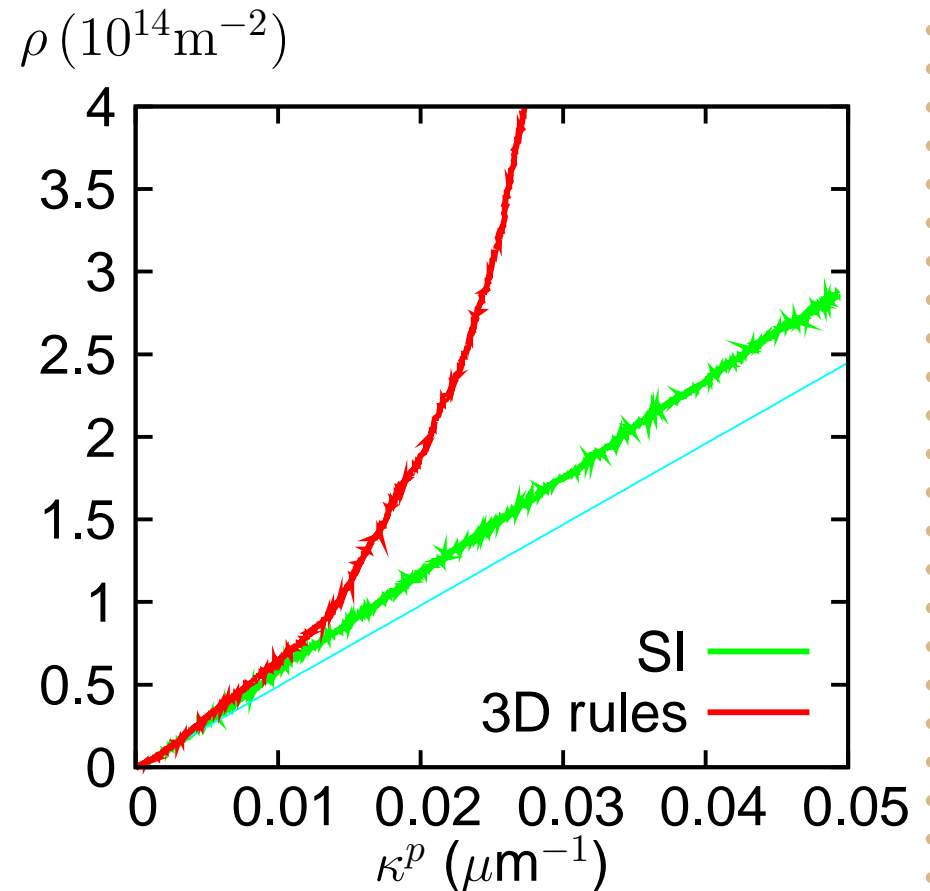
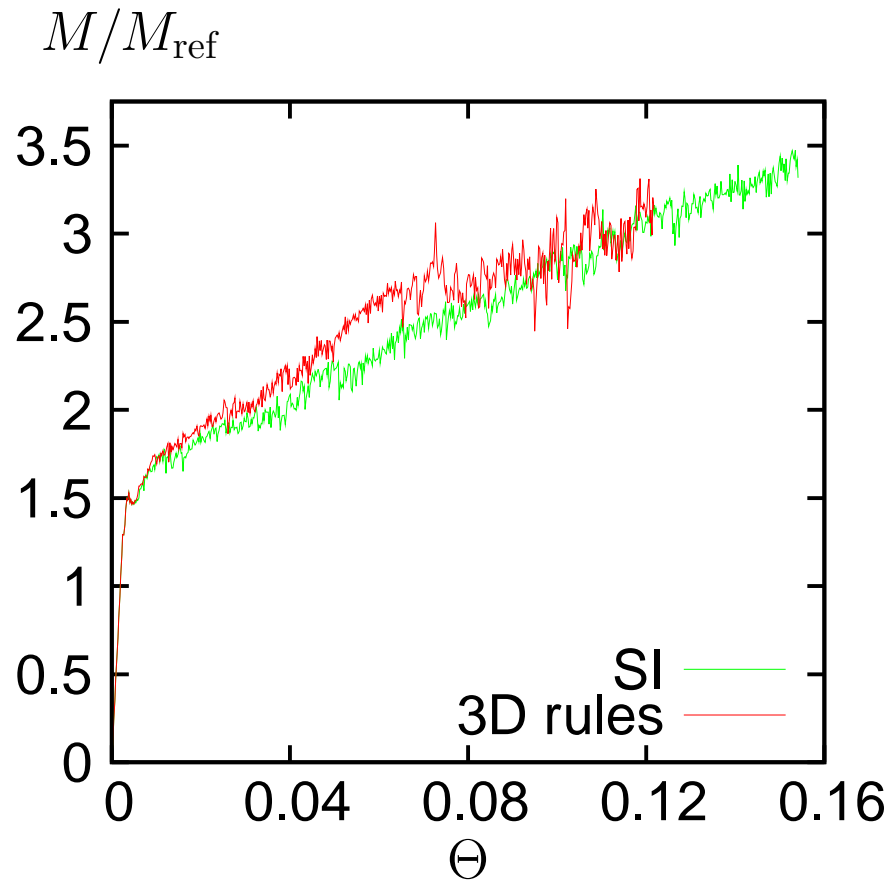


$$\rho_G = \frac{\kappa^p}{b_1} = \frac{\kappa^p}{b \cos(\varphi_0)}$$

Bending (new results)

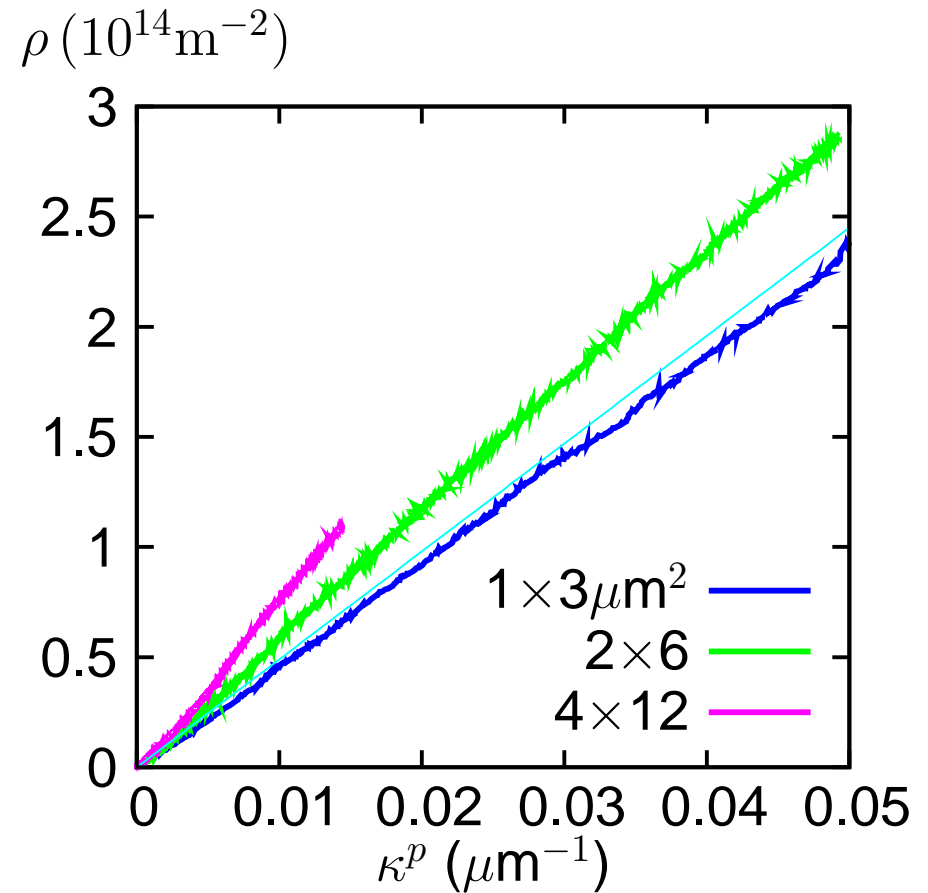
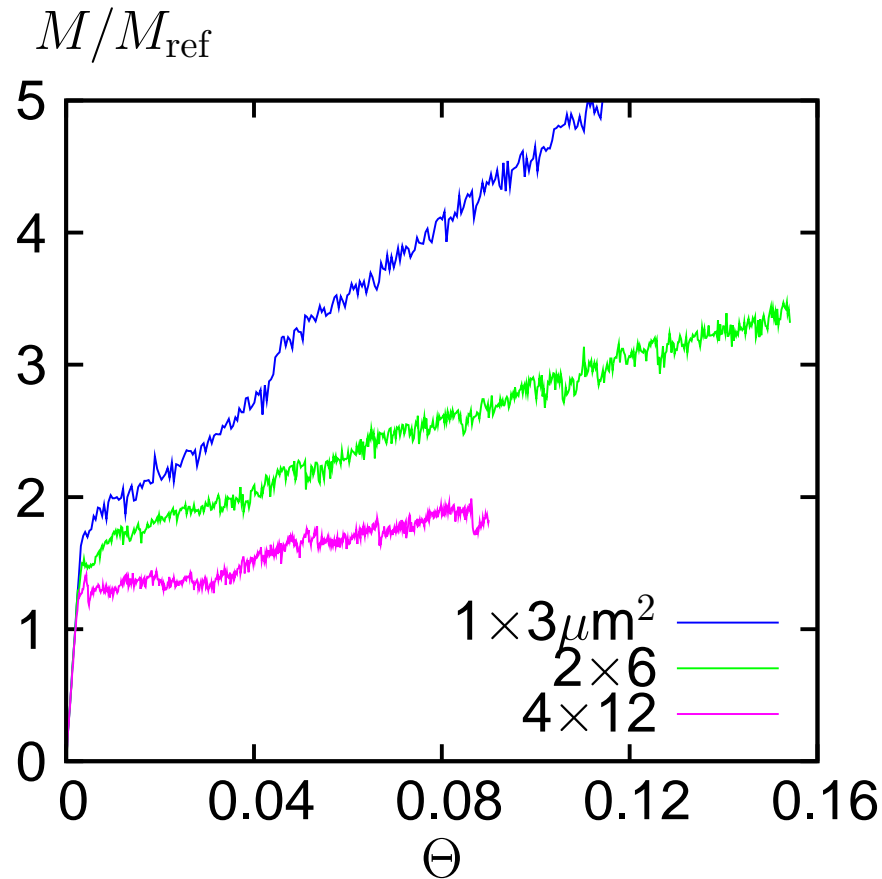


Bending (new results)

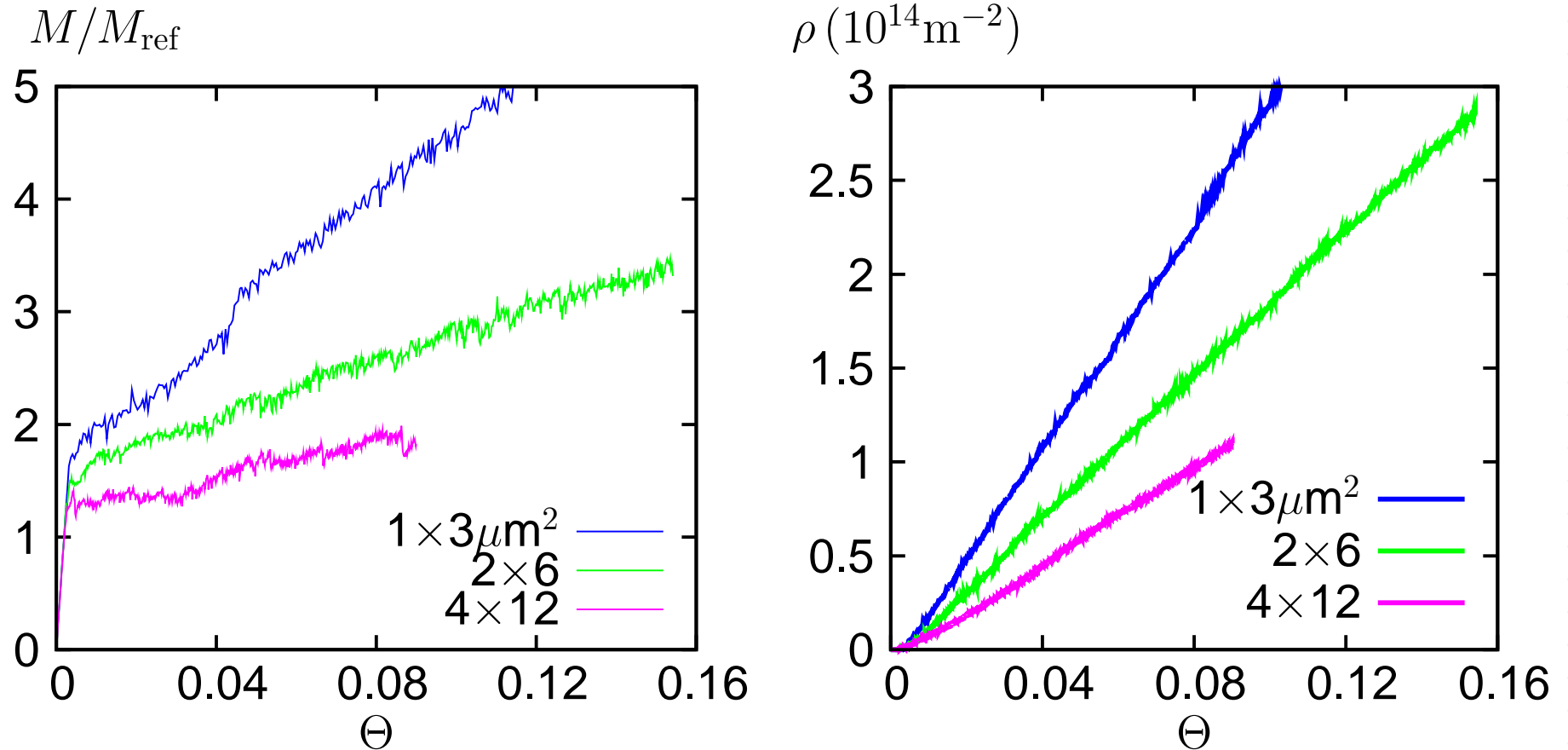


dislocation density is not the only structural parameter governing strength

Bending (new results)

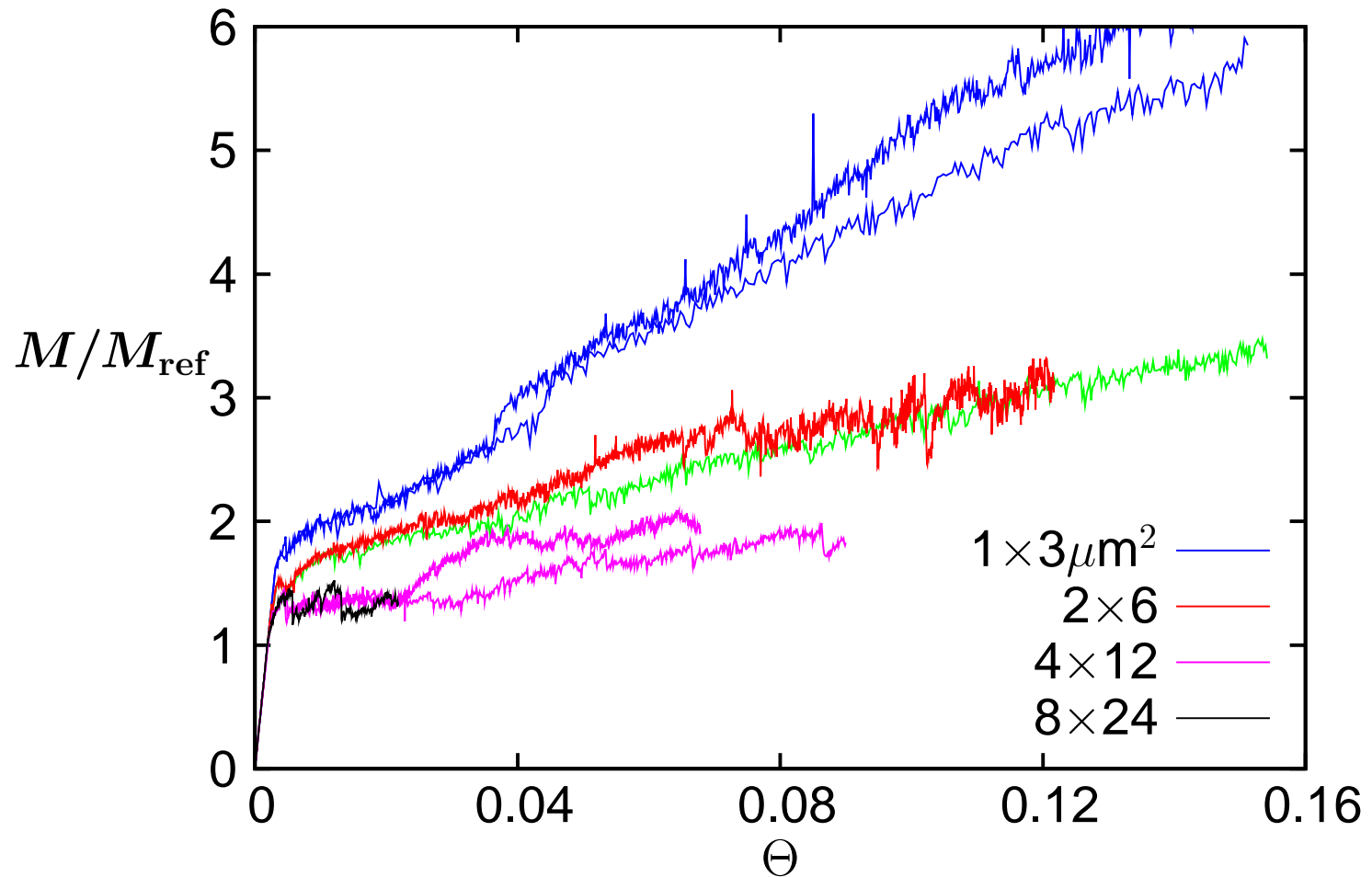


Bending (new results)

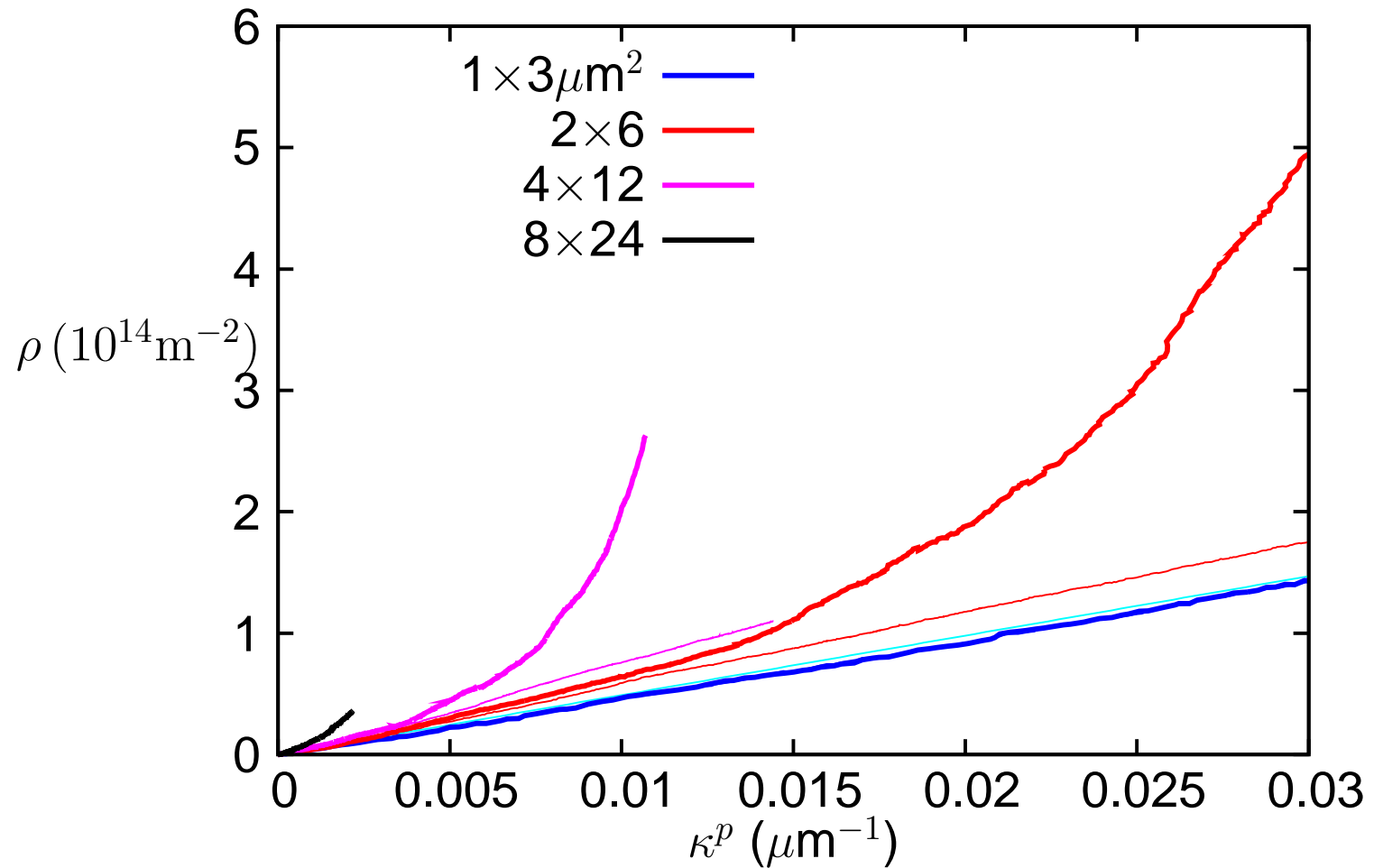


The size effect is seen in M_{yield} and the “hardening”

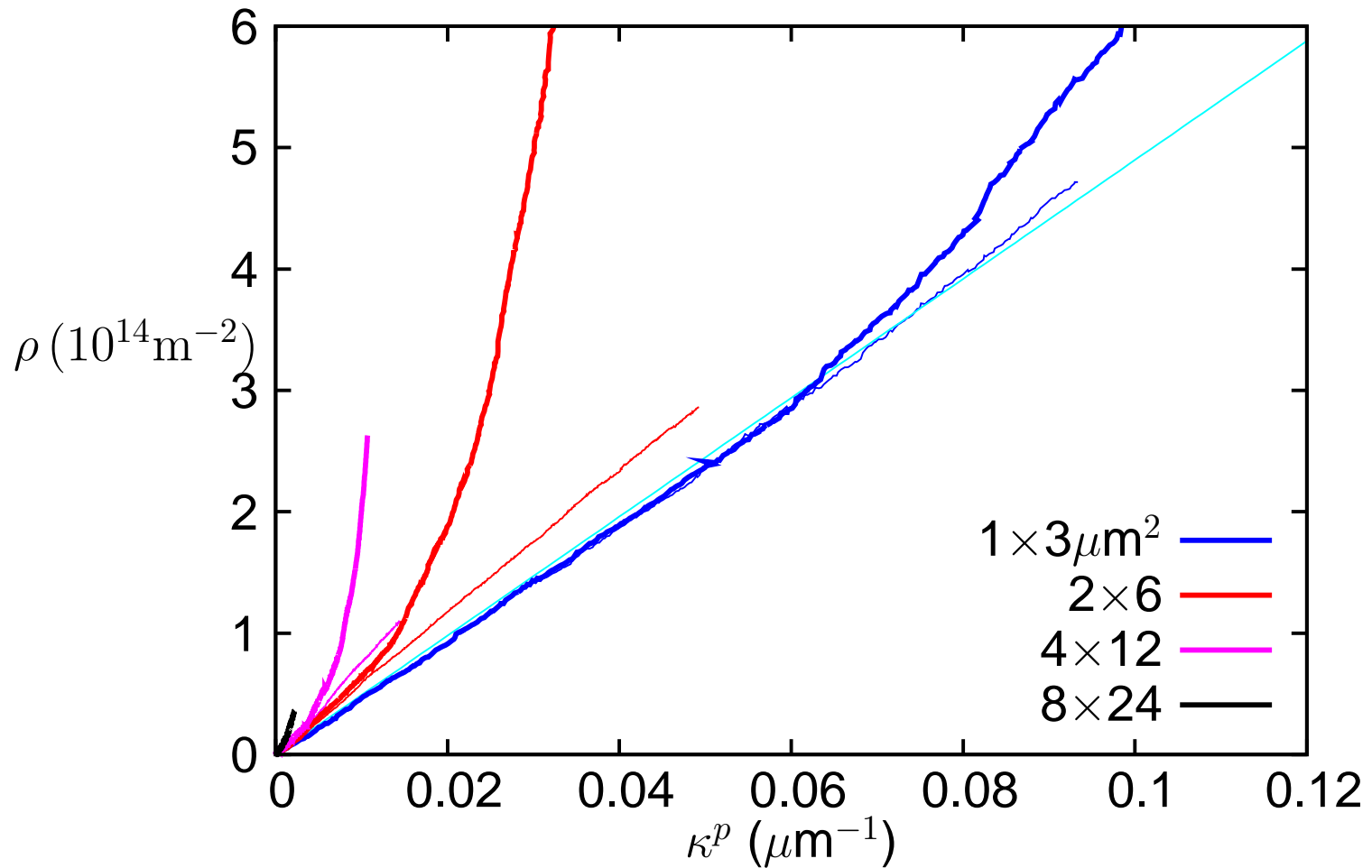
Bending (effect of 3D Rules)



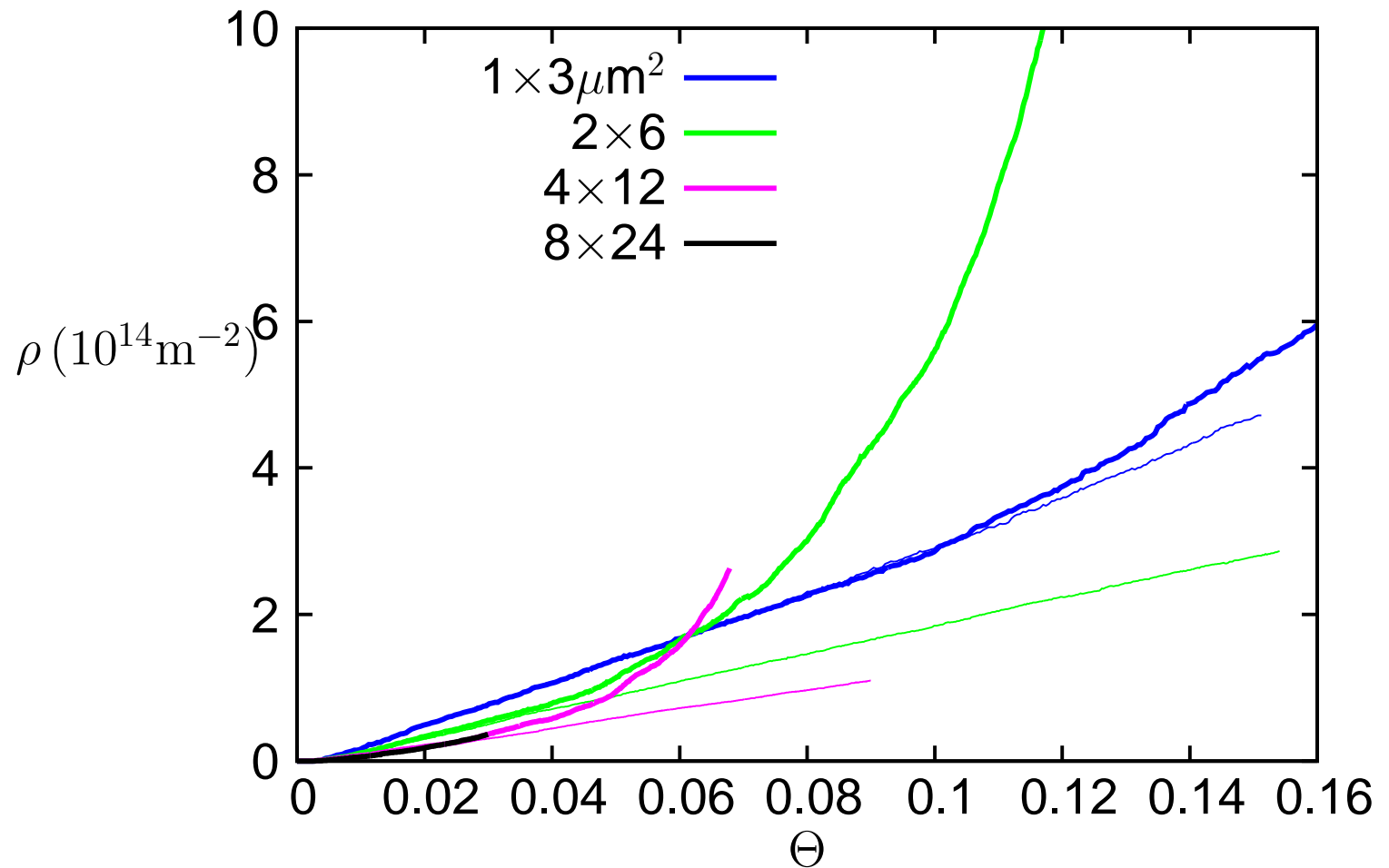
Bending (effect of 3D Rules)



Bending (effect of 3D Rules)



Bending (effect of 3D Rules)



Bending (effect of 3D Rules)

